



IBI Group
400-333 Preston Street
Ottawa, Ontario
K1S 5N4

SANITARY SEWER DESIGN SHEET

PROJECT: FORMER CFB ROCKCLIFFE
LOCATION: CITY OF OTTAWA
CLIENT: CANADA LANDS COMPANY

LOCATION				RESIDENTIAL										ICI AREAS								INFILTRATION ALLOWANCE				TOTAL FLOW (L/s)	PROPOSED SEWER DESIGN						
STREET	AREA ID	FROM MH	TO MH	SF	UNIT TYPES			APT	AREA (Ha)	POPULATION		PEAK FACTOR	PEAK FLOW (L/s)	INSTITUTIONAL		AREA (Ha)		INDUSTRIAL	PEAK FLOW (L/s)	PARKS		FLOW (L/s)	CAPACITY (L/s)	LENGTH (m)	DIA (mm)		SLOPE (%)	VELOCITY (full) (m/s)	AVAILABLE CAPACITY				
					SD	TH/F	TH/S			IND	CUM			IND	CUM	IND	CUM			IND	CUM								L/s	(%)			
PHASE 1 - CODD'S ROAD SHAFT																																	
Major Collector	100A	MH100A	MH (52)					500	3.81	900.0	900.0	3.83	13.96										3.81	3.81	1.07	15.03	84.38	48.00	250	1.85	1.665	69.36	82.19
Major Collector		MH (52)	MH105A							900.0		3.83	13.96																				
Major Collector	105A	MH105A	MH (54)				41		0.77	94.3	994.3	3.80	15.31									0.65	1.42	5.23	1.46	16.78	62.04	62.95	250	1.00	1.224	45.26	72.96
Major Collector		MH (54)	MH (55)							0.0	994.3	3.80	15.31											5.23	1.46	16.78	62.04	50.36	250	1.00	1.224	45.26	72.96
Major Collector		MH (55)	MH108A							0.0	994.3	3.80	15.31											5.23	1.46	16.78	43.87	76.71	250	0.50	0.866	27.09	61.76
Major Collector																																	
Major Collector	COM2	MH126A	MH (379)													2.03	2.03			1.76			2.03	2.03	0.57	2.33	60.47	85.08	250	0.95	1.193	58.14	96.15
Major Collector		MH (379)	MH120A														2.03			1.76				2.03	0.57	2.33	60.47	87.33	250	0.95	1.193	58.14	96.15
Major Collector	COM1	MH120A	MH (402)													2.44	4.47			3.88			2.44	4.47	1.25	5.13	43.87	91.89	250	0.50	0.866	38.74	88.30
Major Collector		MH (402)	MH108A														4.47			3.88				4.47	1.25	5.13	43.87	70.26	250	0.50	0.866	38.74	88.30
---	108A	MH108A	MH (375)						1.32	0.0	994.30	3.80	15.31				4.47			3.88			1.32	11.02	3.09	22.28	54.08	80.08	250	0.76	1.067	31.81	58.81
---		MH (375)	MH (376)							0.0	994.3	3.80	15.31				4.47			3.88				11.02	3.09	22.28	54.08	37.59	250	0.76	1.067	31.81	58.81
---		MH (376)	MH114A							0.0	994.3	3.80	15.31				4.47			3.88				11.02	3.09	22.28	54.08	118.80	250	0.76	1.067	31.81	58.81
---	EXT1	Ex	MH114A						5.53	1574.0	1574.0	3.66	23.36										5.53	5.53	1.55	24.91							
---		MH125A	MH (405)				33			89.1	89.1	4.00	1.44				0.00			0.00				0.00	0.00	1.44	44.30	72.00	250	0.51	0.874	42.86	96.74
---		MH (405)	MH114A							0.0	89.1	4.00	1.44				0.00			0.00				0.00	0.00	1.44	44.30	105.98	250	0.51	0.874	42.86	96.74
---	114A	MH114A	MH (65)				95		1.72	218.5	2786.8	3.47	39.17				4.47			3.88			1.72	18.27	5.12	48.16	71.33	69.47	300	0.50	0.978	23.17	32.48
---		MH (65)	MH (66)							0.0	2786.8	3.47	39.17				4.47			3.88				18.27	5.12	48.16	71.33	81.98	300	0.50	0.978	23.17	32.48
---		MH (66)	MH (67)							0.0	2786.8	3.47	39.17				4.47			3.88				18.27	5.12	48.16	71.33	24.65	300	0.50	0.978	23.17	32.48
---		MH (67)	MH113A							0.0	2786.8	3.47	39.17				4.47			3.88				18.27	5.12	48.16	71.33	10.46	300	0.50	0.978	23.17	32.48
---		MH113A	MH119A							0.0	2786.8	3.47	39.17				4.47			3.88				18.27	5.12	48.16	71.33	52.12	300	0.50	0.978	23.17	32.48
---		MH119A	MH130A							0.0	2786.8	3.47	39.17				4.47			3.88				18.27	5.12	48.16	71.33	72.19	300	0.50	0.978	23.17	32.48
---	INST1, INST2	MH120A	MH125A							0.0	0.0	4.00	0.00	5.55	5.55					4.82			5.55	5.55	1.55	6.37	58.86	191.19	250	0.90	1.162	52.48	89.17
---	125A	MH125A	MH130A				253		3.09	581.9	581.9	3.94	9.29		5.55					4.82			3.09	8.64	2.42	16.52	58.86	176.08	250	0.90	1.162	42.33	71.93
---	163A	MH163A	MH (381)				42		0.75	96.6	96.6	4.00	1.57										0.75	0.75	0.21	1.78	35.64	87.43	250	0.33	0.703	33.86	95.02
		MH (381)	MH130A							0.0	96.6	4.00	1.57											0.75	0.21	1.78	35.64	71.87	250	0.33	0.703	33.86	95.02
---	---	MH130A	MH135A							0.0	3465.3	3.39	47.57		5.55		4.47			8.70				27.66	7.74	64.01	100.18	88.80	375	0.30	0.879	36.18	36.11
---	164A	MH164A	MH (383)				41		0.96	94.3	94.3	4.00	1.53										0.96	0.96	0.27	1.80	35.64	87.27	250	0.33	0.703	33.84	94.96
---		MH (383)	MH135A							0.0	94.3	4.00	1.53											0.96	0.27	1.80	35.64	71.78	250	0.33	0.703	33.84	94.96
---	135A	MH135A	MH140A					191	1.76	343.8	3903.4	3.34	52.86		5.55		4.47			8.70			1.76	30.38	8.51	70.06	100.18	107.95	375	0.30	0.879	30.12	30.07
---	---	MH140A	MH (61)							0.0	3903.4	3.34	52.86		5.55		4.47			8.70				30.38	8.51	70.0.							



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LOCATION				RESIDENTIAL										ICI AREAS										INFILTRATION ALLOWANCE				TOTAL FLOW	PROPOSED SEWER DESIGN						
STREET	AREA ID	FROM MH	TO MH	UNIT TYPES					AREA (Ha)	POPULATION		PEAK FACTOR	PEAK FLOW (L/s)	INSTITUTIONAL		AREA (Ha)		INDUSTRIAL		PEAK FLOW (L/s)	AREA (Ha)			FLOW (L/s)	CAPACITY (L/s)	LENGTH (m)	DIA (mm)	SLOPE (%)	VELOCITY (full) (m/s)	AVAILABLE CAPACITY					
				SF	SD	TH/F	TH/S	APT		IND	CUM			IND	CUM	IND	CUM	IND	CUM		PARKS	IND	CUM							L/s	(%)	L/s	(%)		
Codd's Road	150A	MH155A	MH (411)					285	2.55	513.0	3556.9	3.38	48.68			1.23						0.92	3.47	27.72	7.76	56.44	81.80	105.38	375	0.20	0.717	25.36	31.00		
Codd's Road		MH (411)	MH150A							0.0	3556.9	3.38	48.68			1.23								27.72	7.76	56.44	91.46	65.59	375	0.25	0.802	35.01	38.28		
---		MH150A	MH151A							0.0	7460.3	3.08	93.08		5.55		5.70			9.77		0.00	64.91	18.17	121.02	129.34	30.28	375	0.50	1.134	8.32	6.43			
---	190A	MH190A	MH (358)	4		19			0.96	64.9	64.9	4.00	1.05									0.96	0.96	0.27	1.32	63.27	65.18	250	1.04	1.249	61.95	97.91			
---		MH (358)	MH (359)							0.0	64.9	4.00	1.05										0.96	0.27	1.32	63.27	17.99	250	1.04	1.249	61.95	97.91			
---		MH (359)	MH (360)							0.0	64.9	4.00	1.05										0.96	0.27	1.32	63.27	37.59	250	1.04	1.249	61.95	97.91			
---		MH (360)	MH (361)							0.0	64.9	4.00	1.05										0.96	0.27	1.32	63.27	26.53	250	1.04	1.249	61.95	97.91			
---		MH (361)	MH185A							0.0	64.9	4.00	1.05										0.96	0.27	1.32	63.27	57.21	250	1.04	1.249	61.95	97.91			
---	185A	MH185A	MH (363)			12			0.38	32.4	97.3	4.00	1.58								0.38	1.34	0.38	1.95	35.64	16.83	250	0.33	0.703	33.69	94.52				
---		MH (363)	MH183A							0.0	97.3	4.00	1.58										1.34	0.38	1.95	35.64	64.96	250	0.33	0.703	33.69	94.52			
---	192A	MH192A	MH (364)	39					1.52	132.6	132.6	4.00	2.15									1.52	1.52	0.43	2.57	35.64	89.21	250	0.33	0.703	33.06	92.78			
---		MH (364)	MH190A							0.0	132.6	4.00	2.15										1.52	0.43	2.57	35.64	91.02	250	0.33	0.703	33.06	92.78			
---	EXT2	BULKHEAD	MH190A						8.97	538.2	538.2	3.96	8.63									8.97	8.97	2.51	11.14	35.64	65.00	250	0.33	0.703	24.50	68.74			
---	190A	MH190A	MH179A			9			0.31	24.3	695.10	3.90	10.97									0.31	10.80	3.02	14.00	84.38	78.92	250	1.85	1.665	70.39	83.41			
---	194A	MH194A	MH (356)	24					1.28	81.6	81.6	4.00	1.32									1.28	1.28	0.36	1.68	48.06	105.74	250	0.60	0.948	46.37	96.50			
---		MH (356)	MH179A							0.0	81.6	4.00	1.32										1.28	0.36	1.68	48.06	100.13	250	0.60	0.948	46.37	96.50			
---	179A	MH179A	MH (76)			10			0.34	27.0	803.7	3.86	12.56								0.37	0.71	12.79	3.58	16.15	47.65	43.07	250	0.59	0.940	31.51	66.12			
---		MH (76)	MH183A							0.0	803.7	3.86	12.56										12.79	3.58	16.15	47.65	34.27	250	0.59	0.940	31.51	66.12			
---	183A	MH183A	MH182A	9					0.60	30.6	931.6	3.82	14.41									0.60	14.73	4.12	18.54	31.02	119.22	250	0.25	0.612	12.48	40.23			
---	195A	MH195A	MH182A	14					0.85	47.6	47.6	4.00	0.77									0.85	0.85	0.24	1.01	59.18	107.15	250	0.91	1.168	58.17	98.29			
---	---	MH182A	MH175A							0.0	979.2	3.81	15.10										15.58	4.36	19.46	31.02	76.76	250	0.25	0.612	11.56	37.27			
---	230A, INST3	MH230A	MH (353)			42			1.08	113.4	113.4	4.00	1.84	2.44	2.44					2.12		3.52	3.52	0.99	4.94	51.91	110.31	250	0.70	1.024	46.96	90.48			
---		MH (353)	MH175A							0.0	113.4	4.00	1.84		2.44					2.12			3.52	0.99	4.94	51.91	68.80	250	0.70	1.024	46.96	90.48			
---	175A	MH175A	MH (92)	7					0.52	23.8	1116.4	3.77	17.04		2.44					2.12		0.52	19.62	5.49	24.66	45.12	50.21	300	0.20	0.618	20.46	45.35			
---		MH (92)	MH172A							0.0	1116.4	3.77	17.04		2.44					2.12			19.62	5.49	24.66	45.12	62.97	300	0.20	0.618	20.46	45.35			
---	192A	MH192A	MH (120)	11					0.68	37.4	37.4	4.00	0.61									0.68	0.68	0.19	0.80	43.87	15.79	250	0.50	0.866	43.07	98.18			
---		MH (120)	MH194A							0.0	37.4	4.00	0.61										0.68	0.19	0.80	43.87	66.64	250	0.50	0.866	43.07	98.18			
---	194A	MH194A	MH195A	18					1.43	61.2	98.6	4.00	1.60								1.43	2.11	0.59	2.19	48.06	78.09	250	0.60	0.948	45.87	95.45				
---		MH195A	MH172A							0.0	98.6	4.00	1.60									2.11	0.59	2.19	48.06	77.14	250	0.60	0.948	45.87	95.45				
---		MH172A	MH151A							0.0	1215.0	3.74	18.43		2.44					2.12			21.73	6.08	26.63	45.12	69.18	300	0.20	0.618	18.49	40.98			
---		MH151A	MH (421)								8675.3	3.02	105.98		7.99		5.70			11.88			86.64	24.26	142.12	153.03	124.53	375	0.70	1.342	10.91	7.13			
---		MH (421)	EX Shaft							0.0	8675.3	3.02	105.98		7.99		5.70			11.88		0.00	86.64	24.26	142.12	153.03	9.66	375	0.70	1.342	10.91	7.13			
---	213A	MH213A	MH (374)					89	1.43	160.2	160.2	4.00	2.60									1.43	1.43	0.40	3.00	35.64	56.18	250	0.33	0.703	32.64	91.59			
---		MH (374)	MH211A							0.0	160.2	4.00	2.60										1.43	0.40	3.00	35.64	106.64	250	0.33	0.703	32.64	91.59			
---	---	MH211A	MH217A							0.0	160.2	4.00	2.60										1.43	0.40	3.00	35.64	15.04	250	0.33	0.703	32.64	91.59			
Hemlock Road	230A	MH230A	MH (80)				100		1.51	230.0	230.0	4.00	3.73									1.51	1.51	0.42	4.15	51.16	68.00	250	0.68	1.010	47.01	91.89			
Hemlock Road		MH (80)	MH216A			</																													



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STREET	AREA ID	FROM MH	TO MH	UNIT TYPES				AREA (Ha)	POPULATION		PEAK FACTOR	PEAK FLOW (L/s)	INSTITUTIONAL		AREA (Ha)		INDUSTRIAL	PEAK FLOW (L/s)	AREA (Ha)		FLOW (L/s)	CAPACITY (L/s)	LENGTH (m)	DIA (mm)	SLOPE (%)		VELOCITY (full) (m/s)	AVAILABLE CAPACITY							
				SF	SD	TH/F	TH/S		APT	IND			CUM	IND	CUM	IND			CUM	IND								CUM	L/s	(%)	L/s	(%)			
---	323A	MH323A	MH (12)						0.0	51.3	4.00	0.83								0.47	0.47	1.23	0.34	1.18	87.74	41.89	250	2.00	1.731	86.56	98.66				
---		MH (12)	MH (13)						0.0	51.3	4.00	0.83										1.23	0.34	1.18	87.74	32.20	250	2.00	1.731	86.56	98.66				
---		MH (13)	MH320A						0.0	51.3	4.00	0.83										1.23	0.34	1.18	87.74	27.05	250	2.00	1.731	86.56	98.66				
---	320A	MH320A	MH (15)						0.0	272.7	4.00	4.42			0.00	3.18		2.76	3.44	3.44	10.58	2.96	10.14	72.08	60.67	250	1.35	1.423	61.94	85.93					
---		MH (15)	MH (16)						0.0	272.7	4.00	4.42			0.00	3.18		2.76			10.58	2.96	10.14	72.08	66.68	250	1.35	1.423	61.94	85.93					
---		MH (16)	MH (17)						0.0	272.7	4.00	4.42			0.00	3.18		2.76			10.58	2.96	10.14	72.08	82.93	250	1.35	1.423	61.94	85.93					
---		MH (17)	MH (18)						0.0	272.7	4.00	4.42			0.00	3.18		2.76			10.58	2.96	10.14	72.08	39.16	250	1.35	1.423	61.94	85.93					
---		MH (18)	MH333A						0.0	272.7	4.00	4.42			0.00	3.18		2.76			10.58	2.96	10.14	72.08	29.65	250	1.35	1.423	61.94	85.93					
---	SDA	MH330A	MH331A				275	6.36	495.0	495.0	3.98	7.97									6.36	6.36	1.78	9.75	35.64	132.70	250	0.33	0.703	25.88	72.63				
---		MH331A	MH332A						0.0	495.0	3.98	7.97									0.00	6.36	1.78	9.75	35.64	60.29	250	0.33	0.703	25.88	72.63				
---	332A, AVIATION	MH332A	MH (367)						0.0	495.0	3.98	7.97		AVIATION MUSEUM FIXED FLOW FROM 332A TO NRC SHAFT -->						29.00	2.45	2.45	8.81	2.47	39.44	45.12	48.21	300	0.20	0.618	5.68	12.58			
---		MH (367)	MH (368)						0.0	495.0	3.98	7.97									29.00	0.00	8.81	2.47	39.44	45.12	83.95	300	0.20	0.618	5.68	12.58			
---		MH (368)	MH (369)						0.0	495.0	3.98	7.97									29.00	0.00	8.81	2.47	39.44	45.12	29.01	300	0.20	0.618	5.68	12.58			
---		MH (369)	MH (370)						0.0	495.0	3.98	7.97									29.00	0.00	8.81	2.47	39.44	45.12	42.26	300	0.20	0.618	5.68	12.58			
---		MH (370)	MH338A						0.0	495.0	3.98	7.97									29.00	0.00	8.81	2.47	39.44	45.12	94.01	300	0.20	0.618	5.68	12.58			
---		MH338A	MH333A						0.0	495.0	3.98	7.97									29.00	0.00	8.81	2.47	39.44	45.12	217.08	300	0.20	0.618	5.68	12.58			
---		MH333A	NRC SHAFT						0.0	767.7	3.87	12.04			0.00	3.18		31.76				19.39	5.43	49.23	91.46	35.09	375	0.25	0.802	42.23	46.17				
PHASE 2 - PEACH TREE LANE SHAFT																																			
---	175A	MH175A	MH242A	7					0.69	23.8	23.80	4.00	0.39									0.69	0.69	0.19	0.58	57.20	125.31	250	0.85	1.129	56.62	98.99			
---	242A	MH242A	MH (95)			21			0.68	56.7	80.50	4.00	1.30									0.68	1.37	0.38	1.69	53.73	49.67	250	0.75	1.060	52.04	96.86			
---		MH (95)	MH244A							0.0	80.50	4.00	1.30									0.00	1.37	0.38	1.69	53.73	49.28	250	0.75	1.060	52.04	96.86			
---	235A	MH235A	MH210A			22			0.80	59.4	59.40	4.00	0.96									0.80	0.80	0.22	1.19	48.06	41.66	250	0.60	0.948	46.87	97.53			
---		MH210A	MH244A							0.0	59.40	4.00	0.96									0.00	0.80	0.22	1.19	48.06	78.62	250	0.60	0.948	46.87	97.53			
---	244A	MH244A	MH (105)							0.0	139.90	4.00	2.27							2.64	2.64	4.81	1.35	3.61	58.86	137.40	250	0.90	1.162	55.24	93.86				
---		MH (105)	MH258A							0.0	139.90	4.00	2.27								0.00	4.81	1.35	3.61	58.86	79.88	250	0.90	1.162	55.24	93.86				
---	257A	MH257A	MH256A				158	1.40	284.4	284.40	4.00	4.61									1.40	1.40	0.39	5.00	35.64	68.32	250	0.33	0.703	30.64	85.97				
---	256A	MH256A	MH258A				196	1.45	352.8	637.20	3.92	10.11									1.45	2.85	0.80	10.91	35.64	111.37	250	0.33	0.703	24.73	69.39				
---	258A	MH258A	MH (108)				234		2.83	538.2	1315.30	3.72	19.82								2.83	10.49	2.94	22.76	31.02	32.57	250	0.25	0.612	8.26	26.63				
---		MH (108)	MH (345)							0.0	1315.30	3.72	19.82								0.00	10.49	2.94	22.76	31.02	90.36	250	0.25	0.612	8.26	26.63				
---		MH (345)	MH252A							0.0	1315.30	3.72	19.82								0.00	10.49	2.94	22.76	31.02	11.96	250	0.25	0.612	8.26	26.63				
---	---	MH252A	MH251A							0.0	1315.30	3.72	19.82								0.00	10.49	2.94	22.76	31.02	72.52	250	0.25	0.612	8.26	26.63				
---	256A	MH256A	MH (113)				296	2.65	532.8	532.80	3.96	8.55									2.65	2.65	0.74	9.29	62.04	32.51	250	1.00	1.224	52.75	85.03				
---		MH (113)	MH (114)							0.0	532.80	3.96	8.55								0.00	2.65	0.74	9.29	62.04	31.73	250	1.00	1.224	52.75	85.03				
---		MH (114)	MH (115)							0.0	532.80	3.96	8.55								0.00	2.65	0.74	9.29	62.04	29.65	250	1.00	1.224	52.75	85.03				
---		MH (115)	MH (116)							0.0	532.80	3.96	8.55								0.00	2.65	0.74	9.29	62.04	40.58	250	1.00	1.224	52.75	85.03				
---		MH (116)	MH (117)							0.0	532.80	3.96	8.55								0.00	2.65	0.74	9.29	62.04	35.05	250	1.00	1.224	52.75	85.03				
---		MH (117)	MH251A							0.0	532.80	3.96	8.55								0.00	2.65	0.74	9.29	62.04	22.97	250	1.00	1.224	52.75	85.03				

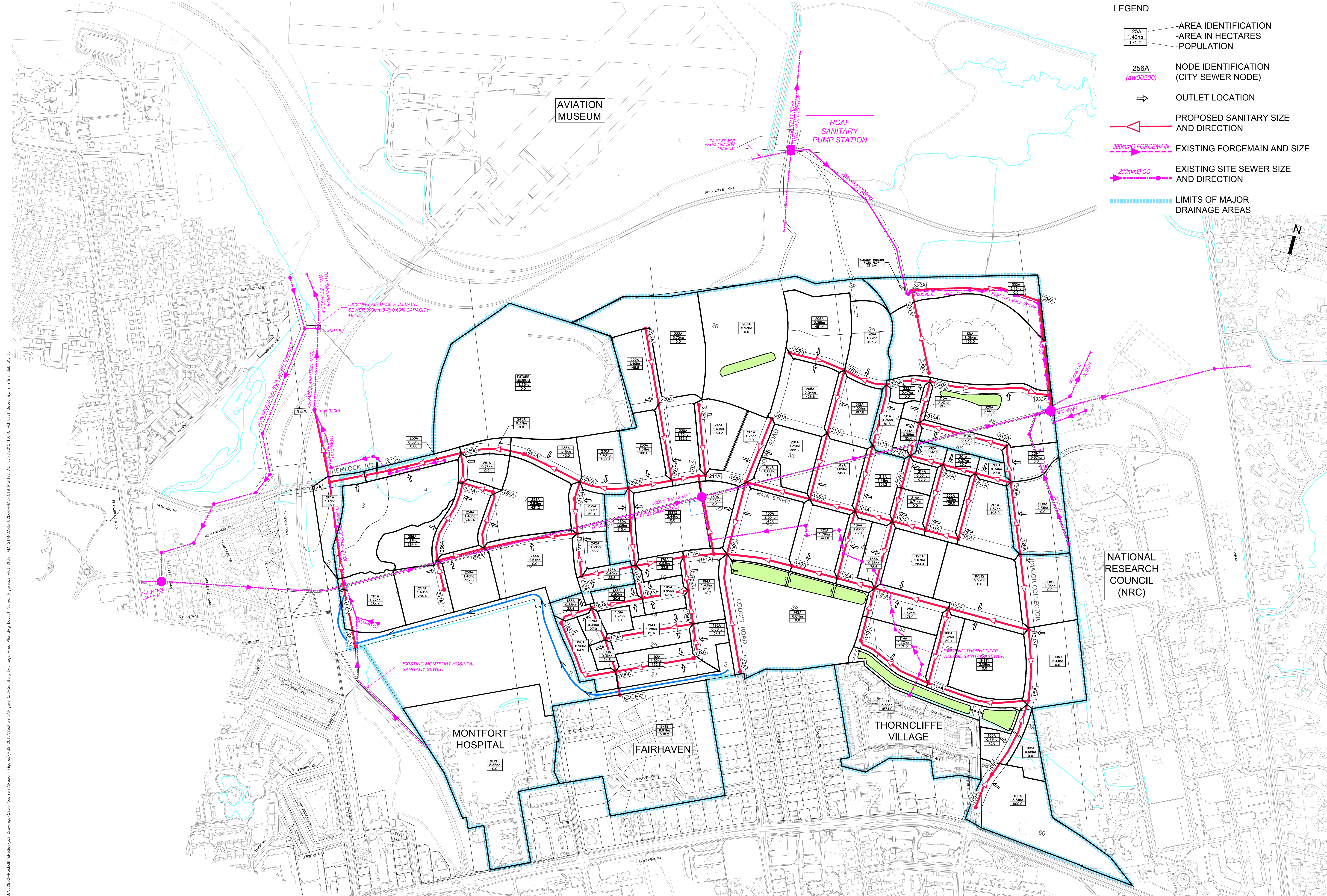
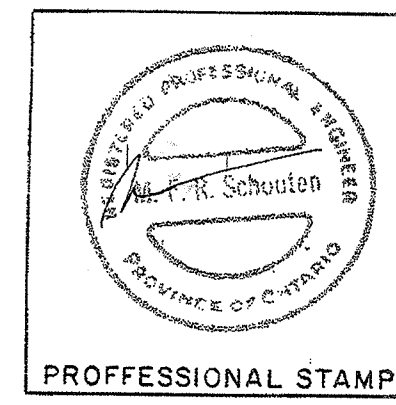


FIGURE 5.2

353 48 15

NO	DATE	REVISION	BY
1	02/05/91	SUBMITTED FOR APPROVAL	M.F.S.
2	31/07/91	SUBMITTED FOR TENDER	M.F.S.



LEGEND

- SANITARY DRAINAGE AREA - DND LANDS
- PROPOSED SANITARY SEWER AND MANHOLE
- AREA TO BE DEVELOPED
- WATERSHED BOUNDARY
- SUB WATERSHED BOUNDARY
- EXISTING STORM SEWER & MANHOLE
- AREA OF SUB WATERSHED
- SUB WATERSHED NUMBER

PROJECT	THORNCLIFFE VILLAGE
TITLE	DND LANDS PROPOSED STORM WATER MANAGEMENT POND AND SANITARY SEWER OUTLET
CLIENT	THORNCLIFFE VILLAGE INC.

J.L. Richards & Associates Limited
Consulting Engineers, Architect & Planners
OTTAWA/KINGSTON, SUBURB, CANADA

SCALE 1:2000 DWG No 12381 SI

TO WEST TRUNK OUTLET

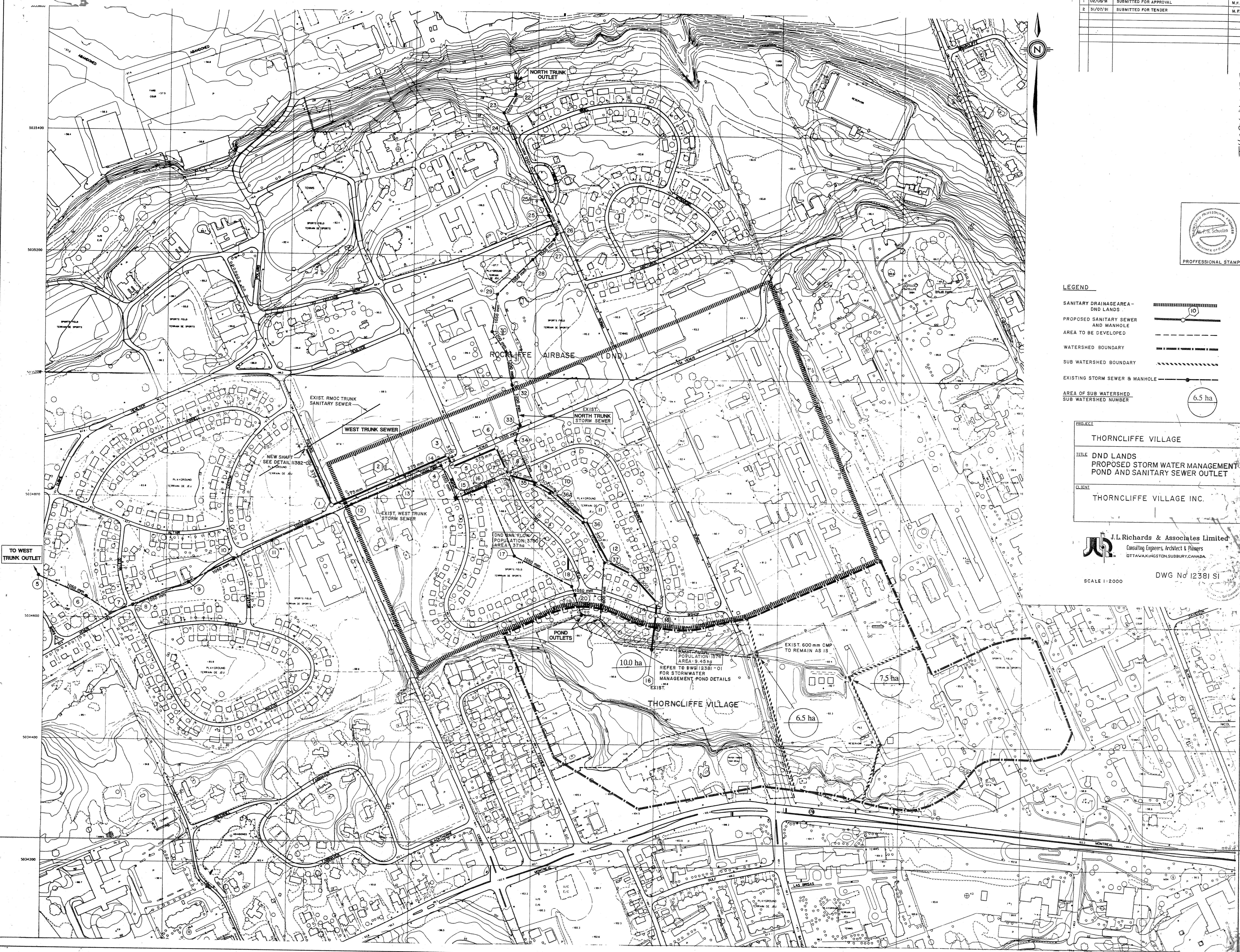
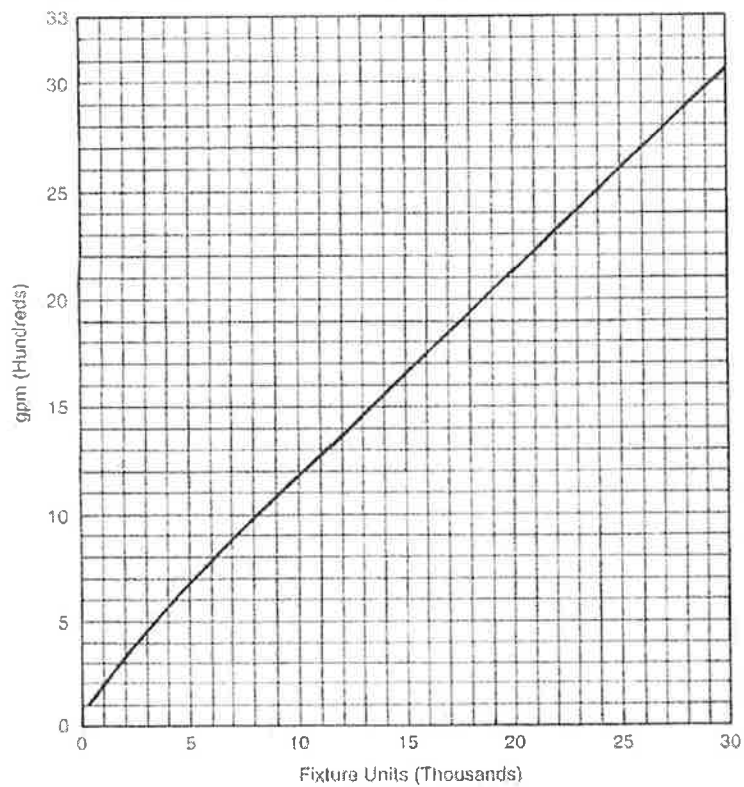


Table 7.5.8.4.
Size and Developed Length of Stack Vents and Vent Stacks
 Forming Part of Sentence 7.5.8.4.(1)

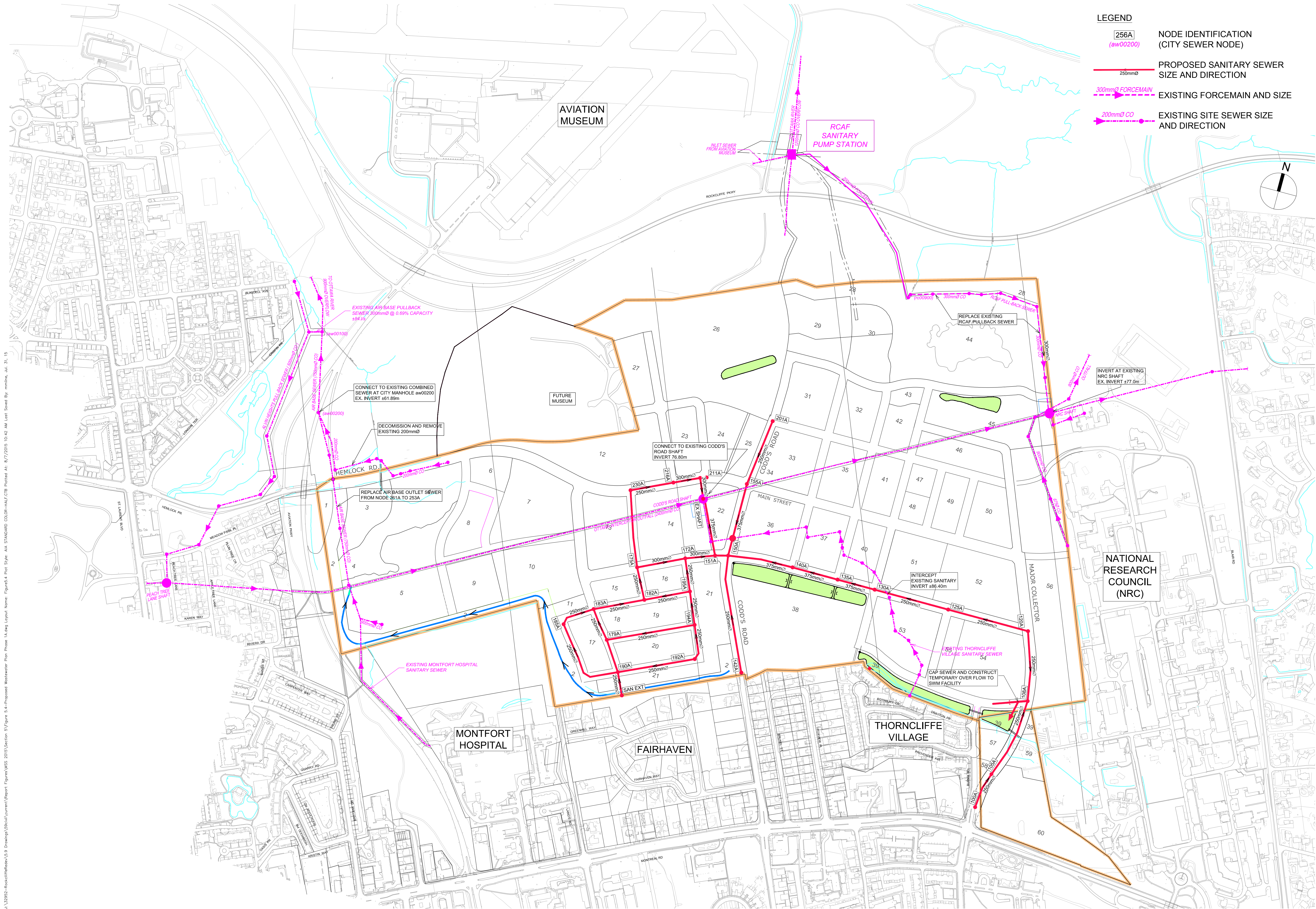
Column 1	Column 2	Column 3	Column 4	Column 5	Column 6	Column 7	Column 8	Column 9	Column 10	Column 11	Column 12	Column 13
Size of Soil or Waste Stack, in.	Total Hydraulic Load Being Vented, fixture units	Water Occupied Area	Size of Stack Vent or Vent Stack, in.									
			1 ¼	1 ½	2	3	4	5	6	8	10	12
			Maximum Length of Stack Vent or Vent Stack, m									
1 ¼	2	0.29	9									
1 ½	8	0.25	15	46								
2	12	0.25	9	23	61							
	24	.29	8	15	46							
3	10	0.15		13	46	317	Not Limited					
	21	.20		10	33.5	247						
	53	.25		8	28.5	207						
	102	.29		7.5	26	189						
4	43	0.15	Not Permitted		10.5	76	299	Not Limited				
	140	.20			8	61	229					
	320	.25			7	52	195					
	540	.29			6.5	46	177					
5	190	0.15	Not Permitted			25	97.5	302	Not Limited			
	490	.20				29	76	232				
	940	.25				16	64	204				
	1 400	.29				15	58	180				
6	500	0.15	Not Permitted			10	39.5	122	305	Not Limited		
	1 100	.20				8	30.5	94.5	238			
	2 000	.25				6.5	25.5	79	201			
	2 900	.29				6	23.5	73	183			
8	1 800	0.15	Not Permitted			9.5	29	73	287	Not Limited		
	3 400	.20				7	22	58	219.5			
	5 600	.25				6	19	49	186			
	7 600	.29				5.5	17	43	70.5			
10	4 000	0.15	Not Permitted					9.5	24	94.5	292.5	Not Limited
	7 200	.20						7	18	73	225.5	
	11 000	.25						6	15.5	61	192	
	15 000	.29						5.5	14	55	174	
12	7 300	0.15	Not Permitted						9.5	36.5	116	287
	13 000	.20							7	28.5	91	219.5
	20 000	.25							6	24	76	186
	26 000	.29							5.5	22	70	152
15	15 000	0.15	Not Permitted							12	39.5	94.5
	25 000	.20								9.5	29	73
	38 000	.25								8	24.5	62
	50 000	.29								7	22.5	55

water piping inside the building up to the point where the connection is taken off to the hot water heater supply.

Figure 13-7 Conversion of Fixture Units to gpm (Mixed System)



A:\30252-Rockcliffe\Drawings\5.9 Drawings\5.9a\Current\Report Figures\MSS 2015\Section 5\Figure 5.4-Proposed Wastewater Plan Phase 1A.dwg, Layout, Name: Figure 5.4-Proposed Wastewater Plan Phase 1A.dwg, Printed At: 8/7/2015 10:42 AM Last Saved By: mmine, Jul, 31, 15



Sheet No.

Drawing Title

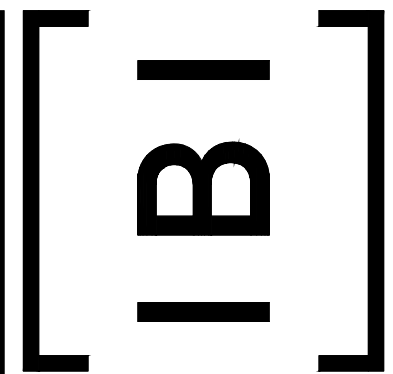
Project Title

Scale

FIGURE 5.4

RECOMMENDED PHASE 1A
WASTEWATER PLAN

FORMER CFB ROCKCLIFFE
MASTER SERVICING STUDY



**CLC Rockcliffe Development
Protection of Interceptor Outfall Sewer and Future Twin
Meeting #2**

**Clyde Avenue Training Room, 1st Floor
January 13, 2017**

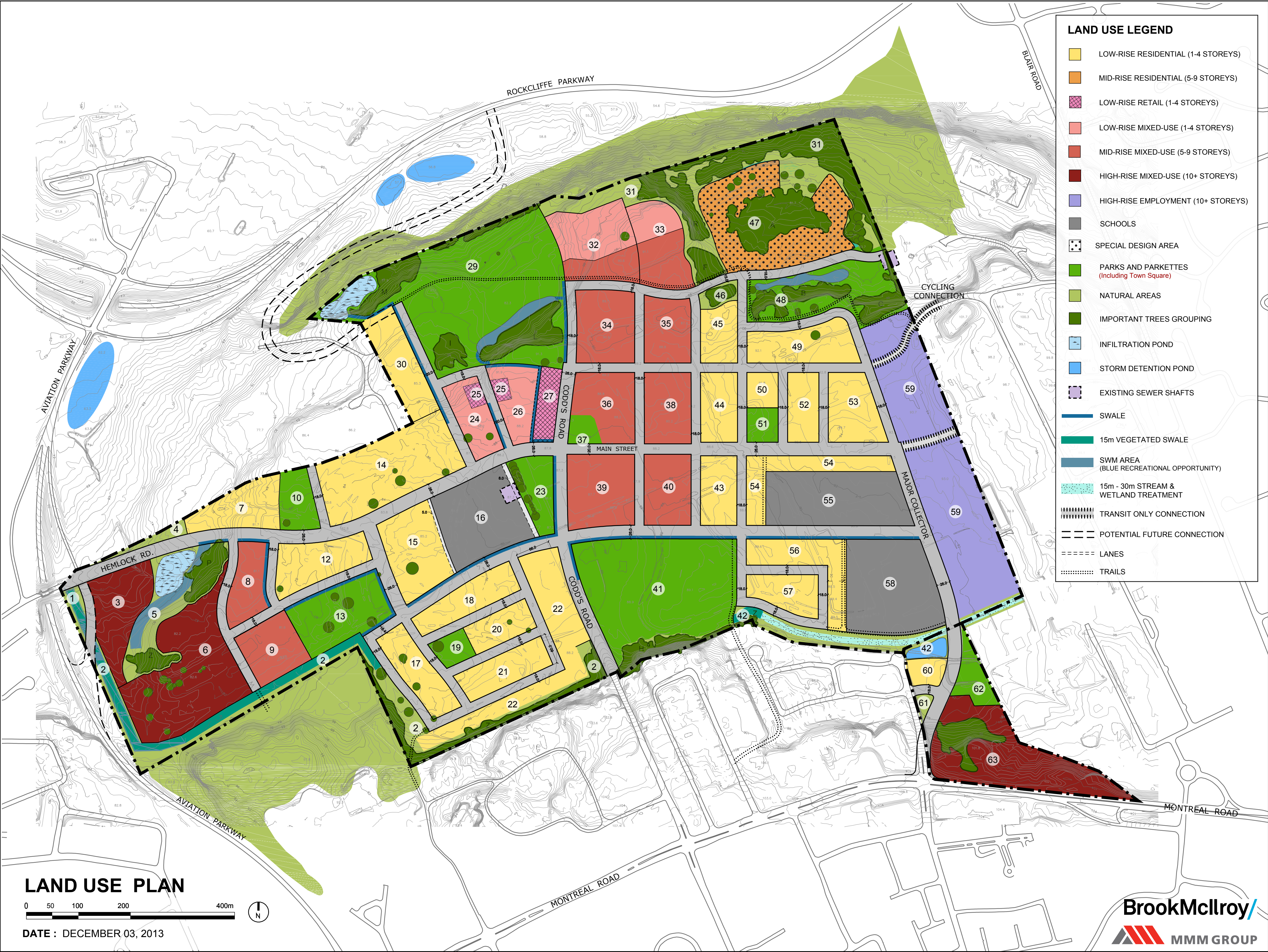
**FINAL MEETING NOTES
(prepared by Chris Rogers)**

In attendance:

Chris Rogers (CR), PGM
Selma Hassan, PGM
Louis Julien, ISD
Shelly McDonald, ESD
Michael Burt, ESD
Gerry Taylor, ESD

	ITEM	ACTION
1	January 7 meeting notes corrections: ISD (Peter McKay) is responsible for setting priority condition assessment of drop shafts, not ISD. IBI (Jim Moffat) requested corrections to minutes on how hydraulic capacity of drop shafts are assessed.	
2	January 7 meeting action item update: SH provided information on existing IOS easement. The easement is not registered. City will work with CLC to have the easement registered as first step. This will also allow CLC to obtain "Absolute Plus Title" and proceed with plan of subdivision. Legal has indicated that a blanket easement for future twin can be secured at the subdivision approval stage. (It is anticipated that the entire CDP study area will be included in a single subdivision application.) LJ is working on establishing a single elevation as a maximum depth of excavation to protect IOS / future twin. SH has added Curtis Rampersad, MB, SM to CLC Rockcliffe TAC.	
3	Draft CDP expected to be circulated in February. There will be a 1 month review period (SH). Drop shaft condition assessment should be completed in about a month so that this information is available to support review of the CDP and MSS. GT suggested that this should be feasible, but winter conditions (fog issues) may cause delays. CR to prompt Peter McKay on making this work a priority.	CR
4	Consideration should be given to maintaining surface easement as well as securing strata easement. Steve Dover (attended meeting briefly) thought that this may have been approach taken for US Embassy, which was built over existing IOS. The ultimate dimensions of the strata easements would likely be slightly larger than indicated in the January 7 meeting minutes (LJ).	

5	Following January 7 meeting, LJ and MB concluded that new IOS shaft is needed due to a lack of staging area around existing shafts. Existing IOS alignment intersects 3 proposed parks in the development area. Suitable area within one of these parks should be planned to allow for <u>temporary use</u> as staging area at any time in future to allow for O&M activities related to the IOS, as well as potential future renewal (relining) work. LJ to confirm area required for these activities, in consultation with CSST consultant and ESD. This area would be also include a <u>permanent</u> access shaft. On the surface, there would be a 2.5m x 2.5m Bilco-type hatch to access the shaft. A large area concrete structure (6m diameter) could be hidden below grade, but no unrelated structures could be built over this area. Alternative locations include the parks located on Block 23 (potentially adjacent to existing drop shaft) and Block 48 (immediately west of existing drop shaft). Blocks shown on attached land use plan (Dec 3, 2013 version). Criteria for selection would be based on input from CLC, City Parks staff, and ESD/ISD staff. Intent would be to plan and construct the new IOS shaft before occupancy of the land in which these blocks are located (candidate locations are not in the Phase 1 development).	LJ
6	Provision for one access shaft for future IOS twin is required. Alternative locations include Blocks 29, 41, and 48. (per Dec 3, 2013 land use plan). Criteria for selection to be established as per proposed shaft for existing IOS. Construction would most likely take place after development and occupancy of surrounding land. Construction staging area required is estimated at ~0.5 ha. LJ to confirm. The construction staging area could include ROW area, and could involve protection of features (e.g. trees) within the staging area. Detailed mitigation and reinstatement requirements would be established in consultation with City Parks staff at the time that plans for the IOS twin shaft are prepared. The IOS twin shaft location could also serve as entry/exit point for tunnel boring machine, in which case construction activities could extend over 18-24 months.	LJ
7	Intent to add blanket strata easement over entire site for future IOS twin at subdivision stage to be added to CDP documentation. CDP should also identify intent to construct 2 shafts, one for IOS and one for future twin, and also identify alternative locations. Detailed design of land use would need to be compatible with needs associated with the shafts as described above. SH to coordinate.	SH



APPENDIX E

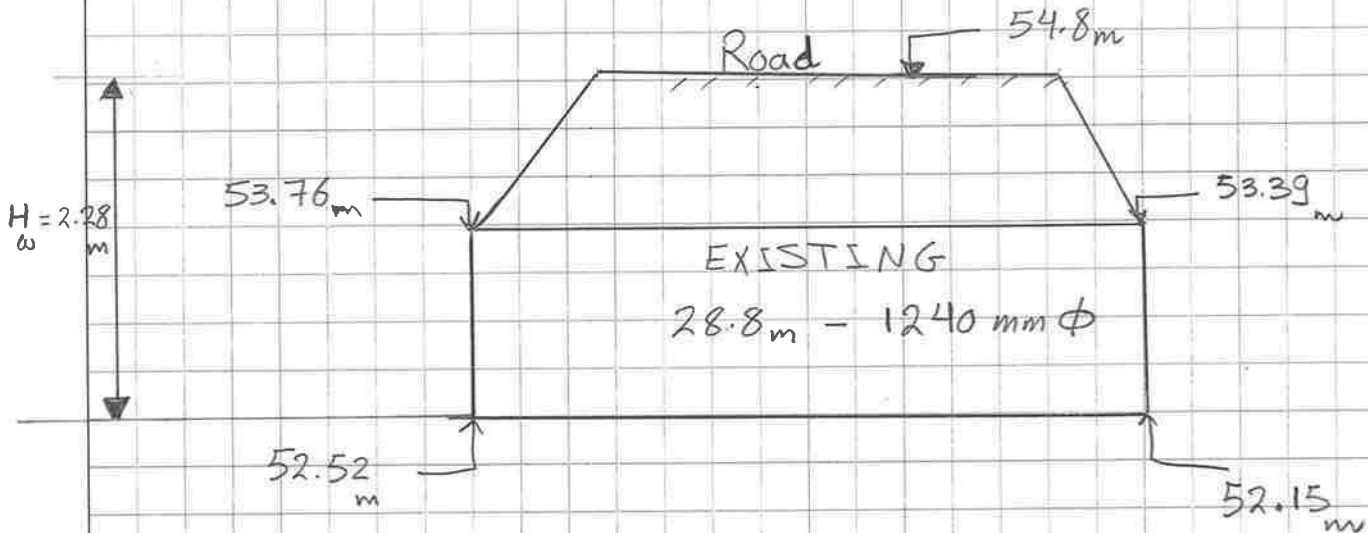
STORMWATER MANAGEMENT SYSTEM: SUPPORTING INFORMATION

- Culvert Design Nomographs – Eastern (Rockcliffe Parkway) Culvert
- Figure 6.7 Recommended Storm Sewer System
- Figure 6.8 Trunk Sewer Profiles
- Figure 6.9 Rational Method Drainage Area Plan
- Figure 6.11 Existing Conditions SWMHYMO Schematic
- Figure 6.12 Post-Development Conditions SWMHYMO Schematic
- Storm Sewer Design Sheets
- Water Quality Volume Calculations
- Figure 6.15 Macro Grading Plan
- Figure 6.16 Sewer Clearance Plan
- Street Segment Velocity x Depth Summary
- Southwest Drainage Channel Design
- NRC Drainage Swale Design
- 25 mm Outflow from Eastern SWM Facility
- 25 mm Outflow from Western SWM Facility
- Baseflow Augmentation to Eastern Creek
- Figure 6.28 Eastern SWM Facility Outlet Pipe Profile
- Boundary Condition for Western Creek Outlet
- Hydraulic Grade Line Summary
- Figure 6.32 Post-Development Conditions XPSWMM Schematic – East
- Figure 6.33 Post-Development Conditions XPSWMM Schematic – West
- Figure 6.34 Recommended Phase 1A Storm Sewer System
- CD with model files and report PDF
 - SWMHYMO – Existing Conditions, Post-Development Conditions, Post-Development Conditions Velocity by Depth
 - XPSWMM – all storm events



PROJECT:	PROJECT NO.: 32952	SHEET: OF:
CLIENT:	PREPARED BY:	DATE: 2014-10
DESCRIPTION: Final	CHECKED BY:	OTHER:

EASTERN CULVERT (ROCKCLIFFE PARKWAY) :



INLET CONTROL :

$$H_w : 54.80 - 52.52 = 2.28 \text{ m}$$

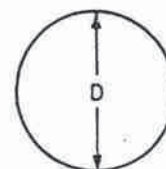
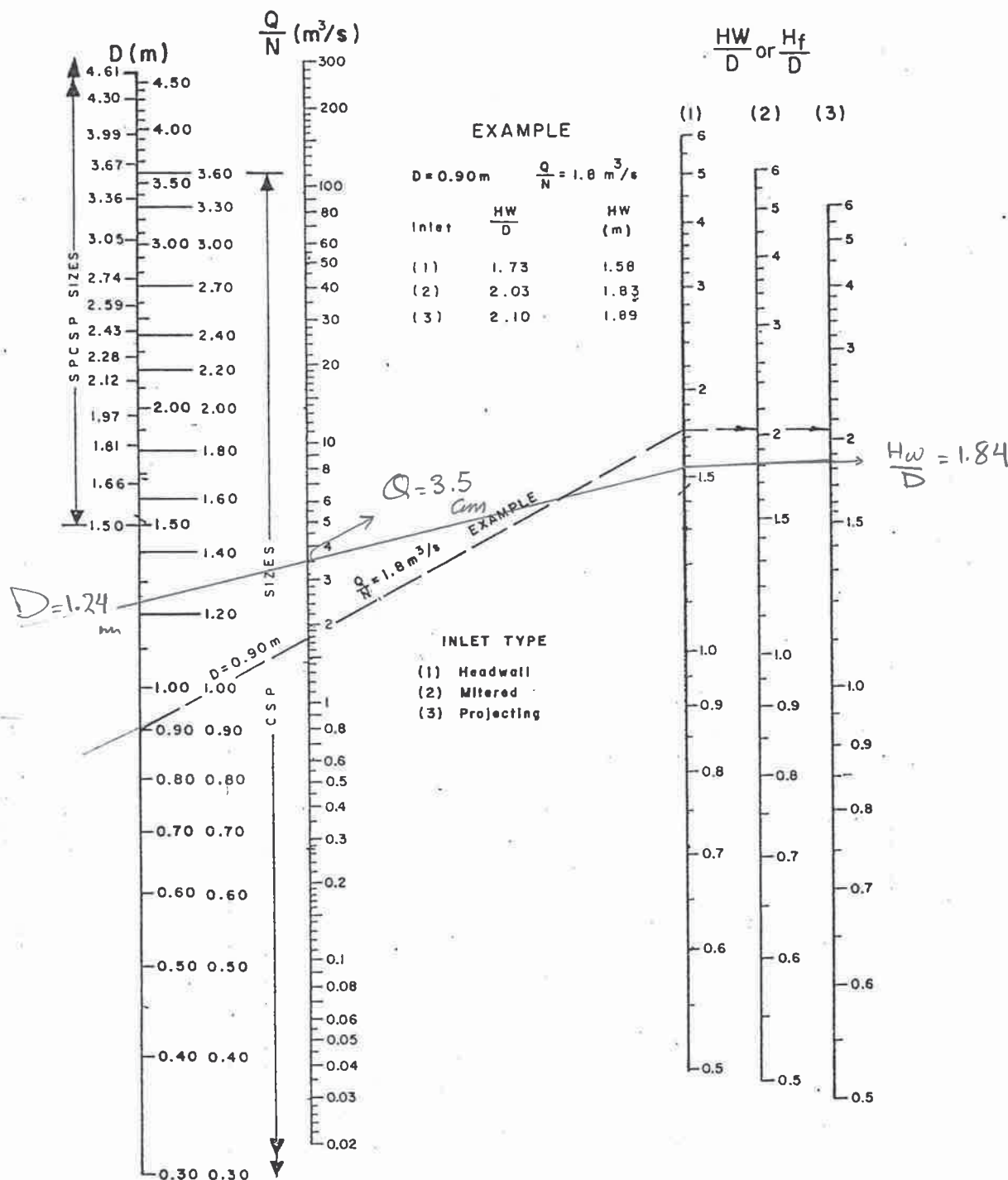
$$\frac{H_w}{D} = \frac{2.28}{1.24} = 1.84 \text{ m} \xrightarrow{\text{Into Design Chart (D5-1G)}} Q = 3.5 \text{ cms}$$

OUTLET CONTROL :

$$H : 53.39 - 54.80 = 1.41 \text{ m} \xrightarrow{\text{Into Design Chart (D5-2C)}} Q = 3.5 \text{ cms}$$
$$D = 1.24 \text{ m}$$

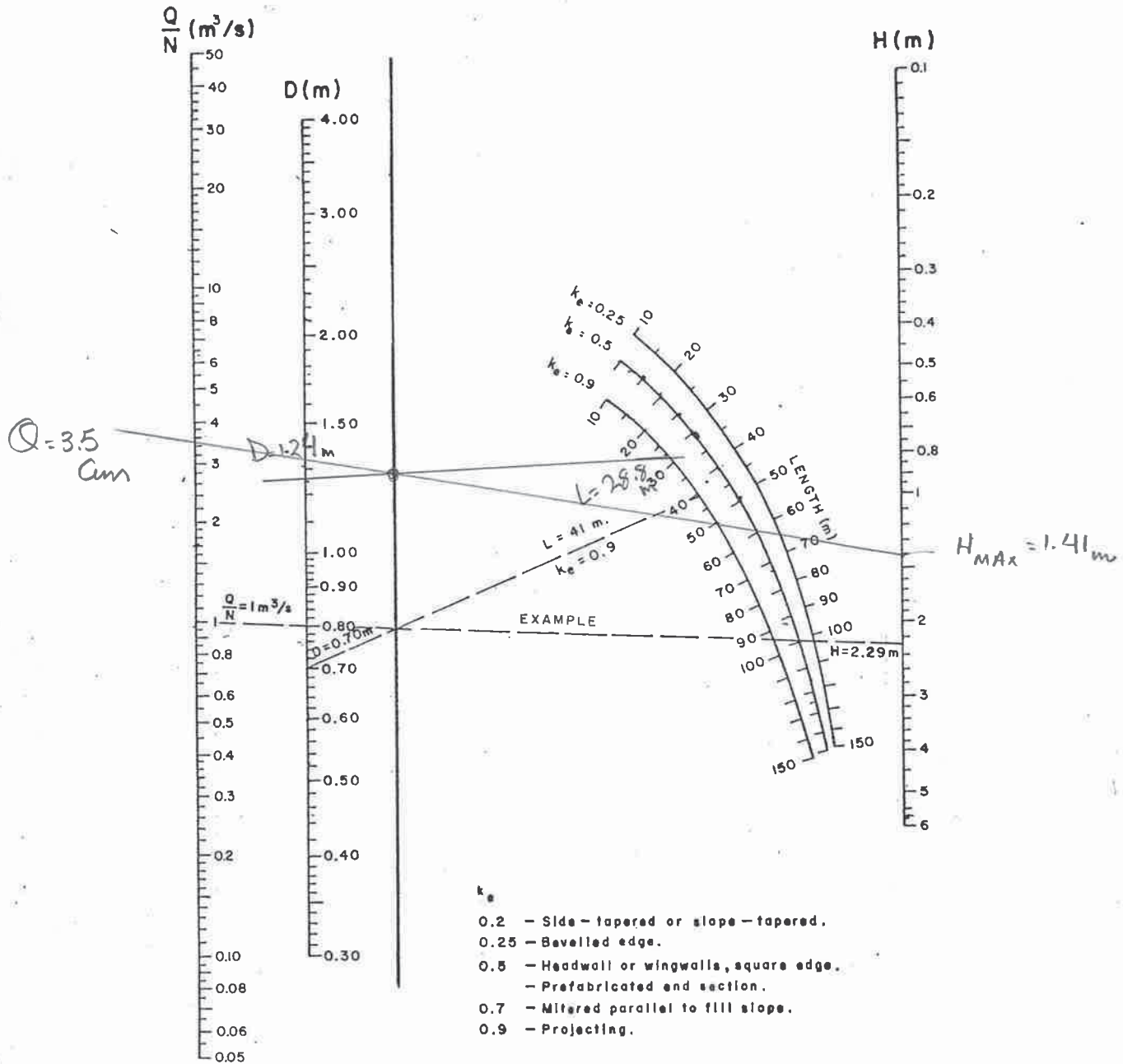
EASTERN

CHART D5-1G

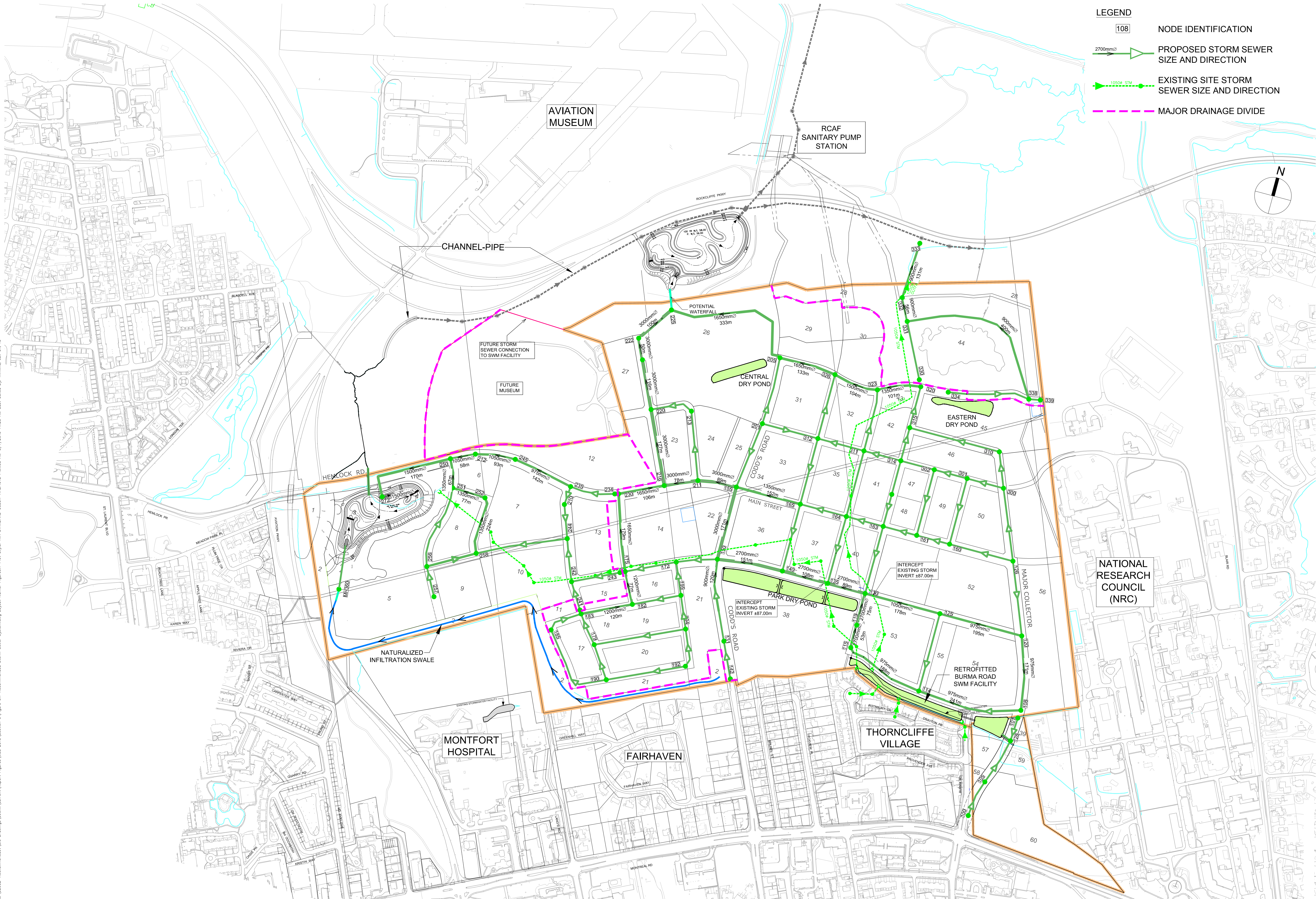


EASTERN

CHART D5-2C



A:\20202-Rockcliffe\Rockcliffe\6.9 Drawings\Sub\Current\Report Figures\MSS 2015 Section 6\Figure 6.7 Recommended Storm Sewer System.dwg Layout Name: Figure6.7 Plot Style: AIA STANDARD COLOR-HALF CTB Printed At: 8/7/2015 11:23 AM Last Saved By: mmh/m, Jul. 31, 15



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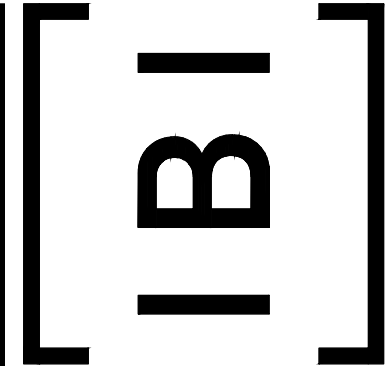
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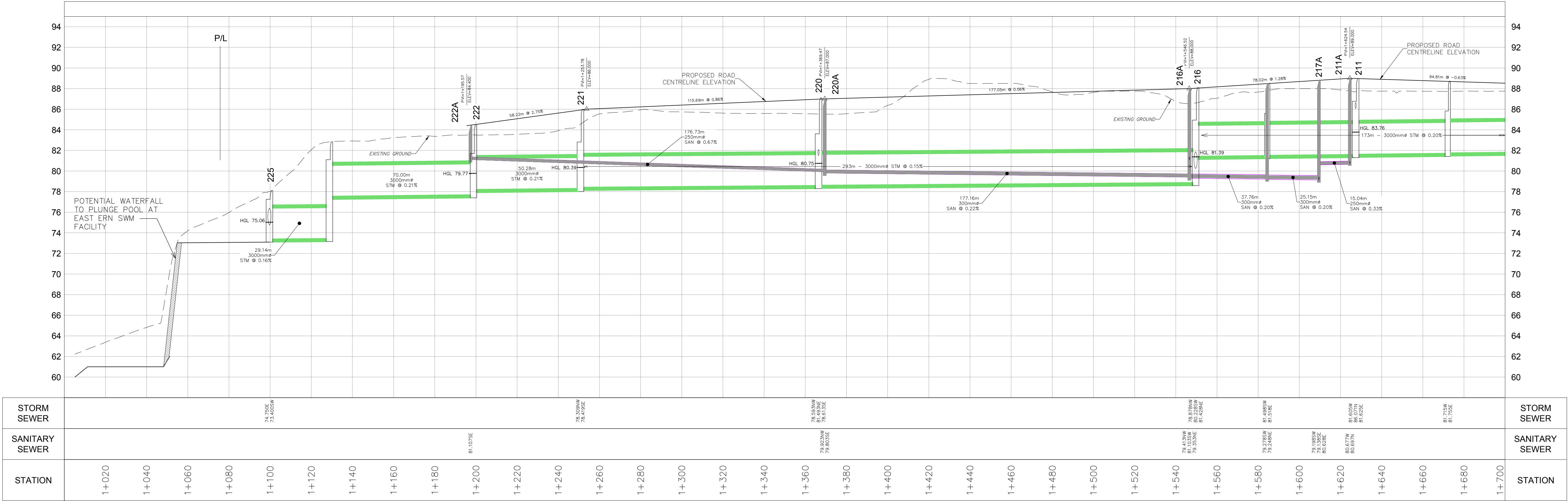
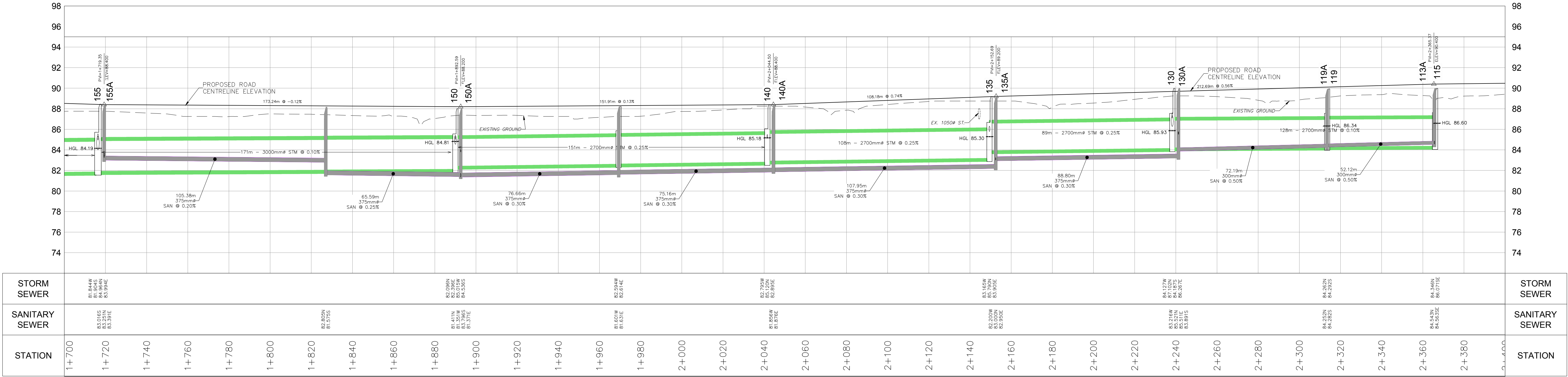
Scale

FIGURE 6.7

RECOMMENDED STORM
SEWER SYSTEM

FORMER CFB ROCKCLIFFE
MASTER SERVICING STUDY





Sheet No.

Drawing Title

Project Title

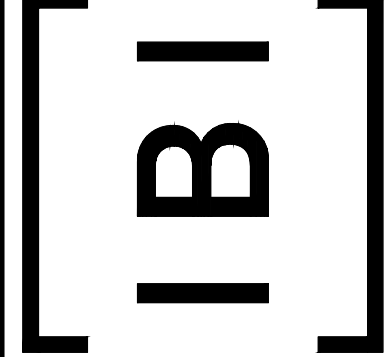
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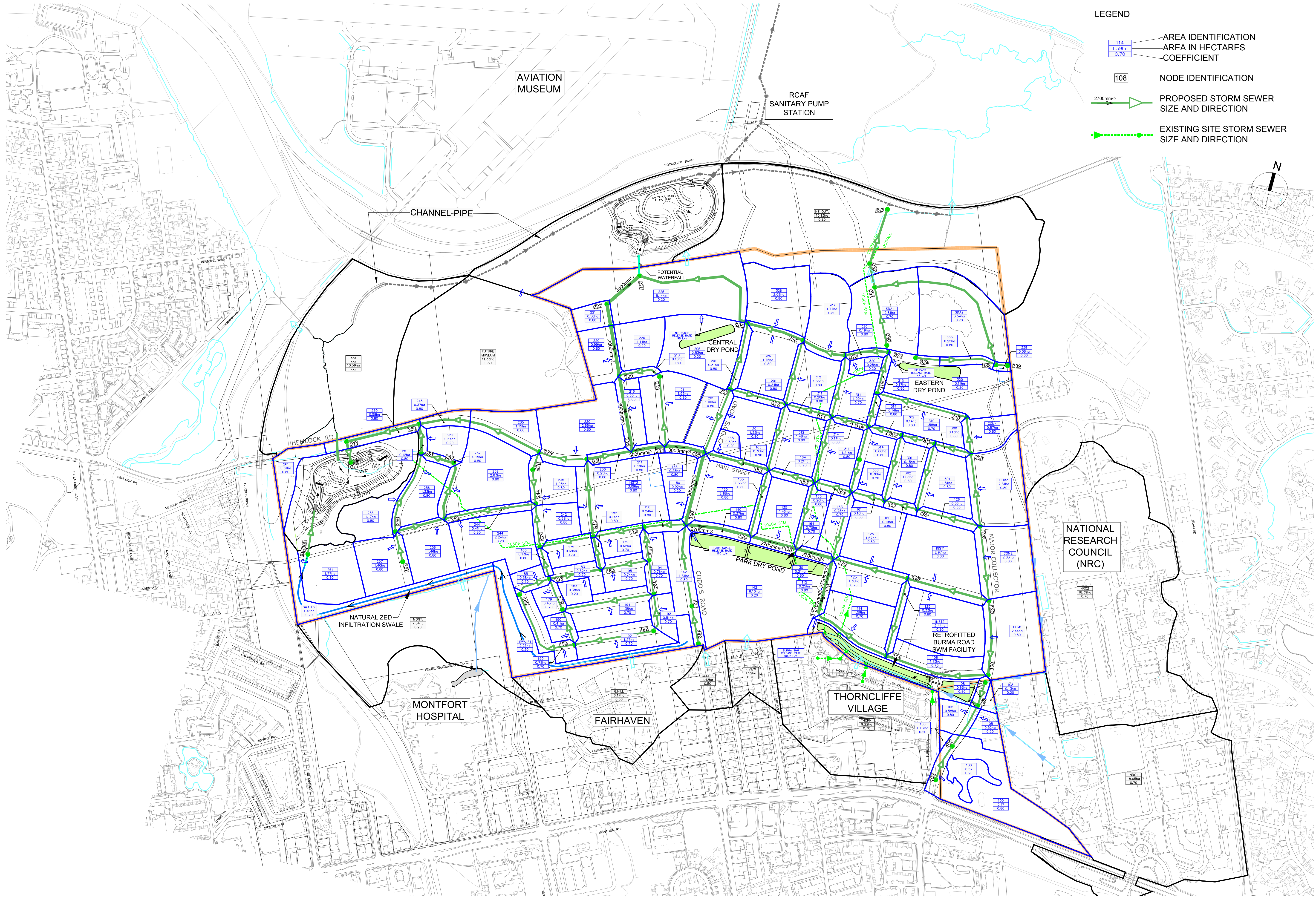
FIGURE 6.8

TRUNK
SEWER PROFILES

FORMER CFB ROCKCLIFFE
MASTER SERVICING STUDY

HORIZ 1:100
VERT 1:100





Sheet No.

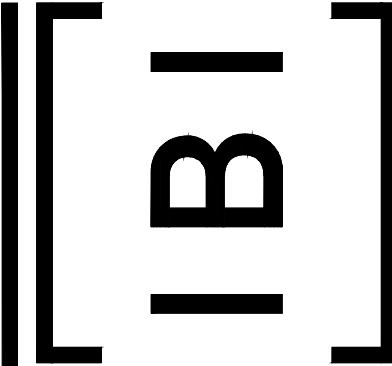
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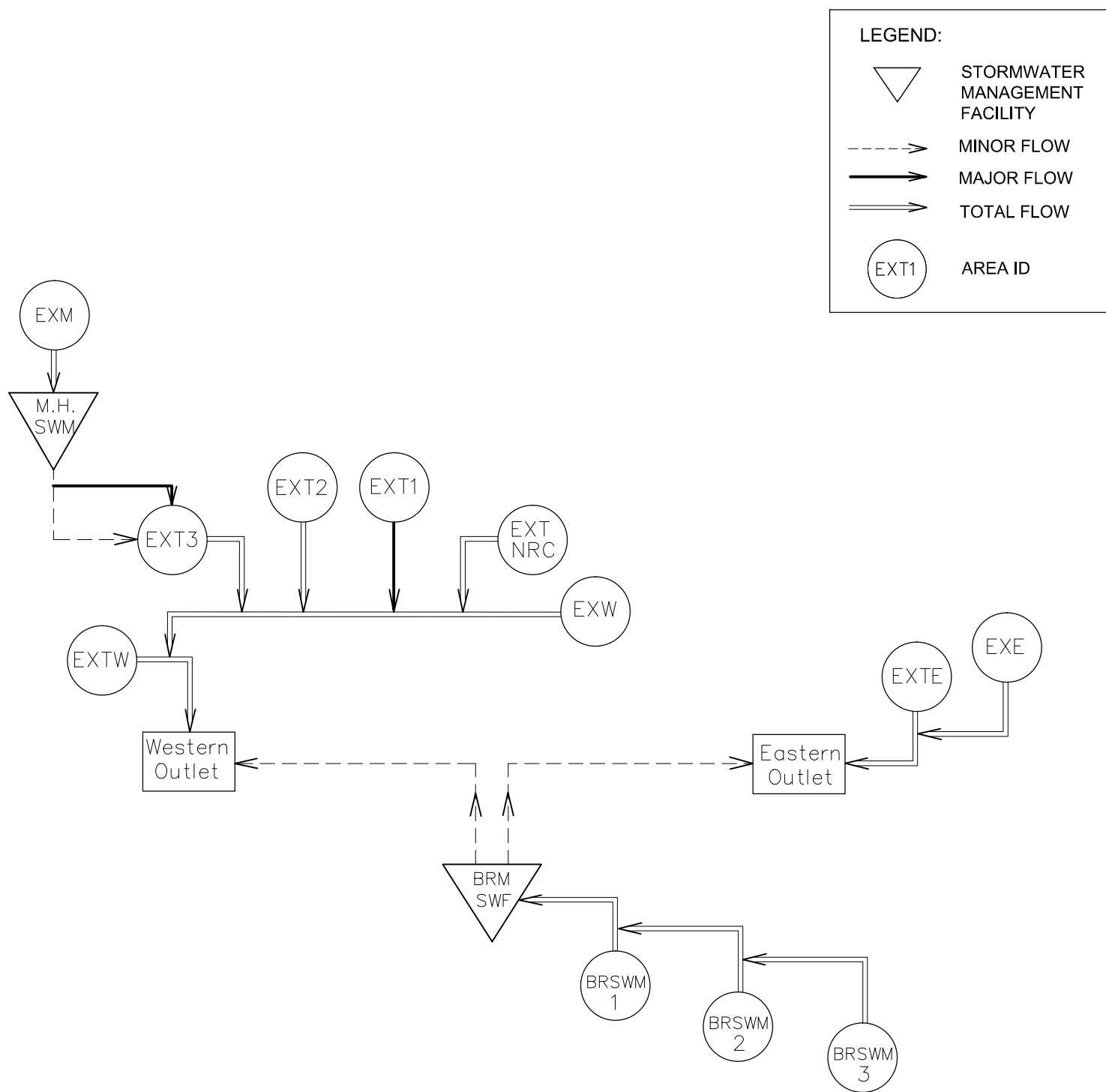
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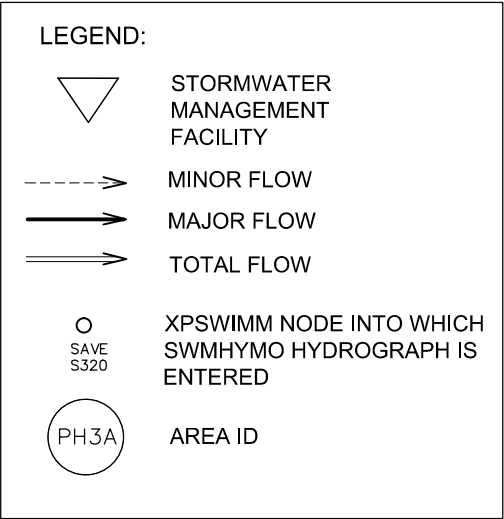
FIGURE 6.9

RATIONAL METHOD
DRAINAGE AREA PLAN
FORMER CFB ROCKCLIFFE
MASTER SERVICING STUDY



J:\32952-RockcliffeRedev\5.9 Drawings\59civil\current\Report Figures\MSS 2015\Section 6\Figure 6.11 Existing Conditions SWMHYMO.dwg Layout Name: Figure6.11







IBI Group
400-333 Preston Street
Ottawa, Ontario
K1S 5N4

STORM SEWER DESIGN SHEET

PROJECT: FORMER CFB ROCKCLIFFE
LOCATION: CITY OF OTTAWA
CLIENT: CANADA LANDS COMPANY

LOCATION				AREA (Ha)						RATIONAL DESIGN FLOW											SEWER DATA										
STREET	AREA ID	FROM MH	TO MH	C=	C=	C=	C=	C=	C=	IND	CUM	INLET (min)	TIME IN PIPE	TOTAL (min)	i (5) (mm/hr)	i (10) (mm/hr)	i (100) (mm/hr)	5yr PEAK FLOW (L/s)	10yr PEAK FLOW (L/s)	FIXED FLOW (L/s)		DESIGN FLOW (L/s)	CAPACITY (L/s)	LENGTH (m)	PIPE SIZE (mm)			SLOPE (%)	VELOCITY (m/s)	AVAIL CAP (5yr)	
				0.20	0.50	0.70	0.75	0.80	0.90											IND	CUM				DIA	W	H			(L/s)	(%)
Major Collector	100	MH100	MH (125)	0.64				3.17		7.41	7.41	10.00	0.28	10.28	104.19	122.14	178.56	771.65			0.00	771.65	871.26	49.50	600			1.85	2.985	99.61	11.43%
Major Collector		MH (125)	MH105							0.00	7.41	10.28	0.21	10.48	102.76	120.45	176.07	761.00			0.00	761.00	871.26	37.24	600			1.85	2.985	110.26	12.66%
Major Collector	105	MH105	MH (127)	0.52				0.58		1.58	8.98	10.48	0.41	10.90	101.70	119.21	174.25	913.79			0.00	913.79	1,161.41	63.10	750			1.00	2.547	247.62	21.32%
Major Collector		MH (127)	MH128							0.00	8.98	10.90	0.31	11.21	99.68	116.83	170.75	895.63			0.00	895.63	1,161.41	48.05	750			1.00	2.547	265.78	22.88%
Major Collector		MH101	MH128	0.13				0.19		0.49	0.49	10.00	1.14	11.14	104.19	122.14	178.56	51.56			0.00	51.56	91.46	55.00	375			0.25	0.802	39.90	43.62%
Major Collector	---	MH128	HW128							0.00	9.48	11.21	0.22	11.43	98.20	115.08	168.19	930.92			0.00	930.92	1,194.45	23.91	900			0.40	1.819	263.53	22.06%
Major Collector	COM2	MH126	MH (310)					2.03		4.51	4.51	10.00	0.67	10.67	104.19	122.14	178.56	470.40			0.00	470.40	624.34	86.13	600			0.95	2.139	153.94	24.66%
Major Collector		MH (310)	MH120							0.00	4.51	10.67	0.67	11.34	100.78	118.12	172.65	454.98			0.00	454.98	624.34	86.49	600			0.95	2.139	169.36	27.13%
Major Collector	COM1	MH120	MH (298)					2.44		5.43	9.94	11.34	1.02	12.36	97.59	114.36	167.13	970.15			0.00	970.15	1,168.98	92.83	975			0.25	1.517	198.82	17.01%
Major Collector		MH (298)	MH108							0.00	9.94	12.36	0.86	13.23	93.17	109.16	159.49	926.18			0.00	926.18	1,168.98	78.49	975			0.25	1.517	242.79	20.77%
---	108	MH108	MH (300)			1.13				2.20	12.14	13.23	0.54	13.77	89.76	105.15	153.60	1,089.69			0.00	1,089.69	1,956.07	82.38	975			0.70	2.538	866.38	44.29%
---		MH (300)	MH (299)							0.00	12.14	13.77	0.25	14.02	87.76	102.80	150.15	1,065.42			0.00	1,065.42	1,956.07	37.87	975			0.70	2.538	890.65	45.53%
---		MH (299)	MH114							0.00	12.14	14.02	0.80	14.81	86.87	101.75	148.62	1,054.66			0.00	1,054.66	1,956.07	121.42	975			0.70	2.538	901.41	46.08%

---	125	MH125	MH (302)					0.33		0.73	0.73	10.00	1.06	11.06	104.19	122.14	178.56	76.47			0.00	76.47	130.62	73.06	375			0.51	1.146	54.16	41.46%
---	---	MH (302)	MH114							0.00	0.73	11.06	1.61	12.67	98.90	115.90	169.39	72.58			0.00	72.58	130.62	110.65	375			0.51	1.146	58.04	44.44%

---	114	MH114	MH (138)			1.59				3.09	15.97	14.81	0.26	15.07	84.16	98.56	143.94	1,343.92			0.00	1,343.92	1,653.18	32.98	975			0.50	2.145	309.26	18.71%
---		MH (138)	MH (139)							0.00	15.97	15.07	0.27	15.34	83.33	97.58	142.50	1,330.63			0.00	1,330.63	1,653.18	35.10	975			0.50	2.145	322.55	19.51%
---		MH (139)	MH (140)							0.00	15.97	15.34	0.64	15.98	82.46	96.57	141.01	1,316.81			0.00	1,316.81	1,653.18	82.05	975			0.50	2.145	336.37	20.35%
---		MH (140)	MH (141)							0.00	15.97	15.98	0.20	16.18	80.52	94.28	137.65	1,285.71			0.00	1,285.71	1,653.18	25.43	975			0.50	2.145	367.47	22.23%
---		MH (141)	MH115							0.00	15.97	16.18	0.10	16.28	79.93	93.59	136.64	1,276.40			0.00	1,276.40	1,653.18	12.64	975			0.50	2.145	376.78	22.79%
---	115	MH115	MH119					0.25		0.56	16.52	16.28	0.47	16.75	79.65	93.25	136.15	1,316.11		9,092.00	9092.00	10,408.11	11,180.46	53.40	2700			0.10	1.892	772.35	6.91%
---		MH119	MH130							0.00	16.52	16.75	0.66	17.41	78.31	91.68	133.84	1,293.97			9092.00	10,385.97	11,180.46	75.21	2700			0.10	1.892	794.50	7.11%

---	INST1, INST2	MH120	MH125					5.41		12.03	12.03	10.00	1.20	11.20	104.19	122.14	178.56	1,253.63			0.00	1,253.63	2,091.13	194.64	975			0.80	2.713	837.49	40.05%
---	125	MH125	MH130			1.30		1.67		6.24	18.28	11.20	1.07	12.26	98.28	115.17	168.32	1,796.05			0.00	1,796.05	2,483.52	177.59	1050			0.76	2.779	687.47	27.68%

---	163	MH163	MH (304)			0.75				1.46	1.46	10.00	1.66	11.66	104.19	122.14	178.56	152.07			0.00	152.07	195.57	87.43	525			0.19	0.875	43.50	22.24%
---		MH (304)	MH130							0.00	1.46	11.66	1.37	13.03	96.15	112.67	164.65	140.33			0.00	140.33	195.57	71.88	525			0.19	0.875	55.23	28.24%

---	130	MH130	MH135					0.21		0.47	36.73	17.41	0.49	17.90	76.50	89.56	130.72	2,809.65		0.00	9092.00	11,901.65	17,677.86	88.81	2700			0.25	2.991	5776.22	32.67%

---	164	MH164	MH (306)			0.75				1.46	1.46	10.00	1.62	11.62	104.19	122.14	178.56	152.07			0.00	152.07	200.65	87.33	525			0.20	0.898	48.58	24.21%
---		MH (306)	MH135							0.00	1.46	11.62	1.33	12.95	96.35	112.90	164.99	140.62			0.00	140.62	200.65	71.77	525						



IBI Group
400-333 Preston Street
Ottawa, Ontario
K1S 5N4

STORM SEWER DESIGN SHEET

PROJECT: FORMER CFB ROCKCLIFFE
LOCATION: CITY OF OTTAWA
CLIENT: CANADA LANDS COMPANY

LOCATION				AREA (Ha)						RATIONAL DESIGN FLOW														SEWER DATA							
STREET	AREA ID	FROM MH	TO MH	C= 0.20	C= 0.50	C= 0.70	C= 0.75	C= 0.80	C= 0.90	IND 2.78AC	CUM 2.78AC	INLET (min)	TIME IN PIPE	TOTAL (min)	i (5) (mm/hr)	i (10) (mm/hr)	i (100) (mm/hr)	5yr PEAK FLOW (L/s)	10yr PEAK FLOW (L/s)	FIXED FLOW (L/s)		DESIGN FLOW (L/s)	CAPACITY (L/s)	LENGTH (m)	PIPE SIZE (mm)			SLOPE (%)	VELOCITY (m/s)	AVAIL CAP (5yr)	
				IND	CUM	DIA	W	H	(L/s)	(%)																					
Main Street	161	MH161	MH163					0.18		0.40	7.34	13.34	0.44	13.78	89.35	104.67	152.90	655.76		0.00	0.00	655.76	1,109.24	79.62	675			1.60	3.003	453.48	40.88%
---	314, 308	MH314	MH308	0.38				0.68		1.72	1.72	10.00	0.61	10.61	104.19	122.14	178.56	179.59			0.00	179.59	358.16	79.88	450			1.45	2.182	178.57	49.86%
---		MH308	MH163							0.00	1.72	10.61	0.59	11.20	101.08	118.47	173.17	174.22			0.00	174.22	351.93	75.98	450			1.40	2.144	177.71	50.50%
Main Street	163	MH163	MH164					0.20		0.44	9.51	13.78	0.49	14.26	87.73	102.76	150.09	834.07		0.00	0.00	834.07	1,105.77	87.42	675			1.59	2.994	271.70	24.57%
---	311	MH311	MH164					1.21		2.69	2.69	10.00	1.34	11.34	104.19	122.14	178.56	280.39			0.00	280.39	318.96	155.81	450			1.15	1.943	38.57	12.09%
Main Street	164	MH164	MH165						0.21	0.53	12.72	14.26	0.80	15.07	86.01	100.74	147.13	1,094.42		0.00	0.00	1,094.42	1,252.90	109.46	825			0.70	2.271	158.48	12.65%
---	312	MH312	MH165					1.48		3.29	3.29	10.00	1.29	11.29	104.19	122.14	178.56	342.95			0.00	342.95	448.66	155.81	525			1.00	2.008	105.70	23.56%
Main Street	165	MH165	MH155	0.30					0.30	0.92	16.93	15.07	1.80	16.86	83.34	97.59	142.52	1,411.17		0.00	0.00	1,411.17	2,083.42	151.92	1350			0.14	1.410	672.25	32.27%
Codd's Road	201	MH201	MH155					2.33		5.18	5.18	10.00	0.93	10.93	104.19	122.14	178.56	539.92			0.00	539.92	822.81	157.13	600			1.65	2.819	282.89	34.38%
Hemlock Road	155	MH155	MH (159)					0.23		0.51	79.17	20.76	0.26	21.02	68.63	80.30	117.15	5,432.88		0.00	9252.00	14,684.88	20,940.87	44.47	3000			0.20	2.870	6256.00	29.87%
Hemlock Road		MH (159)	MH211							0.00	79.17	21.02	0.26	21.28	68.09	79.68	116.23	5,390.65			9252.00	14,642.65	20,940.87	45.30	3000			0.20	2.870	6298.22	30.08%
Hemlock Road	211	MH211	MH (161)					0.19		0.42	79.59	21.28	0.25	21.53	67.56	79.05	115.31	5,376.94			9252.00	14,628.94	20,940.87	43.34	3000			0.20	2.870	6311.94	30.14%
Hemlock Road		MH (161)	MH216							0.00	79.59	21.53	0.20	21.73	67.06	78.46	114.45	5,336.97			9252.00	14,588.97	20,940.87	34.81	3000			0.20	2.870	6351.91	30.33%
---	190	MH190	MH (276)			0.78				1.52	1.52	10.00	0.52	10.52	104.19	122.14	178.56	158.15			0.00	158.15	231.37	63.61	375			1.60	2.029	73.21	31.64%
---		MH (276)	MH (277)							0.00	1.52	10.52	0.17	10.69	101.51	118.98	173.92	154.08			0.00	154.08	231.37	20.18	375			1.60	2.029	77.28	33.40%
---		MH (277)	MH (278)							0.00	1.52	10.69	0.32	11.01	100.69	118.02	172.50	152.84			0.00	152.84	231.37	38.64	375			1.60	2.029	78.53	33.94%
---		MH (278)	MH (279)							0.00	1.52	11.01	0.22	11.22	99.17	116.22	169.86	150.52			0.00	150.52	231.37	26.40	375			1.60	2.029	80.84	34.94%
---		MH (279)	MH185							0.00	1.52	11.22	0.48	11.70	98.15	115.03	168.11	148.98			0.00	148.98	231.37	58.52	375			1.60	2.029	82.38	35.61%
---	185	MH185	MH (281)			0.38				0.74	2.26	11.70	0.32	12.02	95.98	112.47	164.36	216.67			0.00	216.67	300.45	19.48	600			0.22	1.029	83.78	27.89%
---		MH (281)	MH183							0.00	2.26	12.02	1.02	13.04	94.62	110.87	162.00	213.59			0.00	213.59	300.45	63.18	600			0.22	1.029	86.86	28.91%
---	192	MH192	MH (283)			1.27				2.47	2.47	10.00	1.30	11.30	104.19	122.14	178.56	257.50			0.00	257.50	332.84	89.00	600			0.27	1.140	75.34	22.64%
---		MH (283)	MH190							0.00	2.47	11.30	1.39	12.69	97.79	114.60	167.48	241.68			0.00	241.68	332.84	95.19	600			0.27	1.140	91.16	27.39%
---	190	MH190	MH179			0.41				0.80	3.27	12.69	0.47	13.17	91.84	107.60	157.20	300.25			0.00	300.25	871.26	85.03	600			1.85	2.985	571.00	65.54%
---	194	MH194	MH (286)			1.35				2.63	2.63	10.00	1.21	11.21	104.19	122.14	178.56	273.73			0.00	273.73	347.53	112.65	525			0.60	1.555	73.80	21.24%
---		MH (286)	MH179							0.00	2.63	11.21	1.07	12.28	98.22	115.11	168.23	258.04			0.00	258.04	347.53	100.19	525			0.60	1.555	89.49	25.75%
---	179	MH179	MH (209)			0.43				0.84	6.73	13.17	0.33	13.50	89.99	105.42	154.00	605.92		0.00	0.00	605.92	892.10	39.25	750			0.59	1.956	286.18	32.08%
---		MH (209)	MH183							0.00	6.73	13.50	0.32	13.82	88.74	103.94	151.84	597.47			0.00	597.47	892.10	37.55	750			0.59	1.956	294.63	33.03%
---	183	MH183	MH182	0.38		0.52				1.22	10.21	13.82	1.65	15.47	87.57	102.57	149.82	894.43		0.00	0.00	894.43	1,408.95	119.58	1200			0.12	1.207	514.53	36.52%

---	195	MH195	MH182			0.74				1.44	1.44	10.00	1.09	11.09	104.19	122.14	178.56	150.04			0.00	150.04	283.73	113.34	450			0.91	1.728	133.69	47.12%

---	182	MH182	MH175					0.14		0.31	11.97	15.47	0.92	16.39	82.06	96.09	140.31	981.88		0.00	0.00	981.88	1,626.92	77.03	1200			0.16	1.394	645.04	39.65%
---	192	MH192	MH(121)			0.51				0.99	0.99	10.00	0.27	10.27	104.19	122.14	178.56	103.41			0.00	103.41	129.34	18.24	375			0.50	1.134	25.93	20.05%
---		MH(121)	MH194							0.00	0.99	10.27	1.04	11.31	102.80	120.50	176														



IBI Group
400-333 Preston Street
Ottawa, Ontario
K1S 5N4

STORM SEWER DESIGN SHEET

PROJECT: FORMER CFB ROCKCLIFFE
LOCATION: CITY OF OTTAWA
CLIENT: CANADA LANDS COMPANY

LOCATION				AREA (Ha)						RATIONAL DESIGN FLOW												SEWER DATA										
STREET	AREA ID	FROM MH	TO MH	C= 0.20	C= 0.50	C= 0.70	C= 0.75	C= 0.80	C= 0.90	IND 2.78AC	CUM 2.78AC	INLET (min)	TIME IN PIPE	TOTAL (min)	i (5) (mm/hr)	i (10) (mm/hr)	i (100) (mm/hr)	5yr PEAK FLOW (L/s)	10yr PEAK FLOW (L/s)	FIXED FLOW (L/s)		DESIGN FLOW (L/s)	CAPACITY (L/s)	LENGTH (m)	PIPE SIZE (mm)			SLOPE (%)	VELOCITY (m/s)	AVAIL CAP (5yr)		
																					IND	CUM				DIA	W	H				
---	211	MH211	MH (297)					1.93		4.29	4.29	10.00	0.99	10.99	104.19	122.14	178.56	447.23			0.00	447.23	516.44	105.62	600				0.65	1.769	69.21	13.40%
---		MH (297)	MH213							0.00	4.29	10.99	0.51	11.51	99.22	116.28	169.95	425.87			0.00	425.87	516.44	54.28	600				0.65	1.769	90.57	17.54%
---	213	MH213	MH (294)					0.18		0.40	4.69	11.51	0.19	11.69	96.86	113.50	165.87	454.52			0.00	454.52	640.56	24.75	600				1.00	2.195	186.04	29.04%
---		MH (294)	MH (295)							0.00	4.69	11.69	0.23	11.92	96.02	112.52	164.43	450.60			0.00	450.60	640.56	30.15	600				1.00	2.195	189.96	29.66%
---		MH (295)	MH220							0.00	4.69	11.92	0.34	12.26	95.03	111.35	162.70	445.92			0.00	445.92	640.56	44.98	600				1.00	2.195	194.64	30.39%

---	220	MH220	MH221	1.14				0.99		2.84	112.57	22.92	0.78	23.70	64.43	75.37	109.92	7,252.30		0.00	9252.00	16,504.30	18,135.33	115.67	3000				0.15	2.485	1631.03	8.99%
---	221	MH221	MH222					0.50		1.11	113.68	23.70	0.28	23.98	63.06	73.76	107.56	7,168.13			9252.00	16,420.13	21,458.01	50.28	3000				0.21	2.941	5037.87	23.48%
---		MH222	MH (194)							0.00	113.68	23.98	0.40	24.38	62.57	73.19	106.72	7,112.73			9252.00	16,364.73	21,458.01	70.00	3000				0.21	2.941	5093.28	23.74%
---		MH (194)	MH225							0.00	113.68	24.38	0.13	24.51	61.90	72.41	105.58	7,037.17		0.00	9252.00	16,289.17	21,458.01	22.14	3000				0.21	2.941	5168.84	24.09%
---	300	MH300	MH301					0.15		0.33	0.33	10.00	1.78	11.78	104.19	122.14	178.56	34.76			0.00	34.76	133.02	86.45	450				0.20	0.810	98.26	73.87%
---	301	MH301	MH302					0.15		0.33	0.67	11.78	1.60	13.38	95.65	112.08	163.79	63.82			0.00	63.82	133.02	78.00	450				0.20	0.810	69.20	52.02%
---	302	MH302	MH314					0.14		0.31	0.98	13.38	0.99	14.37	89.17	104.46	152.59	87.26			0.00	87.26	220.58	79.44	450				0.55	1.344	133.32	60.44%
---	314	MH314	MH311					0.14		0.31	1.29	14.37	0.81	15.17	85.66	100.32	146.52	110.49			0.00	110.49	297.43	87.56	450				1.00	1.812	186.95	62.85%
---	311	MH311	MH312					0.20		0.44	1.73	15.17	1.01	16.18	83.00	97.20	141.93	143.98			0.00	143.98	297.43	109.47	450				1.00	1.812	153.45	51.59%
---	201	MH201	MH312					0.24		0.53	0.53	10.00	2.37	12.37	104.19	122.14	178.56	55.61			0.00	55.61	67.67	131.93	300				0.45	0.927	12.06	17.82%
---	312	MH312	MH326					1.35		3.00	5.27	16.18	2.41	18.59	79.93	93.58	136.63	421.28		0.00	0.00	421.28	579.98	151.78	825				0.15	1.051	158.70	27.36%
Major Collector	COM3	MH126	MH300					2.31		5.14	5.14	10.00	2.01	12.01	104.19	122.14	178.56	535.29			0.00	535.29	636.13	168.48	750				0.30	1.395	100.85	15.85%
Major Collector	COM4	MH300	MH310					0.87		1.93	7.07	12.01	0.66	12.67	94.64	110.89	162.04	669.32			0.00	669.32	971.71	84.22	750				0.70	2.131	302.38	31.12%
Major Collector	310	MH310	MH (178)			1.58				3.07	10.15	12.67	0.70	13.37	91.92	107.69	157.34	932.72			0.00	932.72	1,296.87	98.01	825				0.75	2.350	364.15	28.08%
Major Collector		MH (178)	MH315							0.00	10.15	13.37	0.81	14.18	89.23	104.53	152.70	905.46			0.00	905.46	1,296.87	114.82	825				0.75	2.350	391.42	30.18%
---	314	MH314	MH315					0.14		0.31	0.31	10.00	0.72	10.72	104.19	122.14	178.56	32.44			0.00	32.44	92.02	78.38	250				2.20	1.816	59.58	64.74%
																						0.00										
---	315	MH315	MH320					0.17		0.38	10.84	14.18	0.55	14.73	86.30	101.08	147.63	935.18		0.00	0.00	935.18	1,640.43	97.47	825				1.20	2.973	705.25	42.99%
---	320	MH320	MH (182)	3.39				0.19		2.31	13.14	14.73	0.35	15.07	84.45	98.90	144.43	1,109.97		147.20	147.20	1,257.17	1,760.81	24.77	1350				0.10	1.192	503.64	28.60%
---		MH (182)	MH (183)							0.00	13.14	15.07	0.46	15.53	83.32	97.57	142.48	1,095.14			147.20	1,424.34	1,760.81	32.67	1350				0.10	1.192	518.48	29.45%
---		MH (183)	MH323							0.00	13.14	15.53	0.60	16.13	81.88	95.88	140.00	1,076.23			147.20	1,223.43	1,760.81	43.11	1350				0.10	1.192	537.39	30.52%
---	311	MH311	MH (321)			1.00				1.95	1.95	10.00	1.01	11.01	104.19	122.14	178.56	202.76			0.00	202.76	311.95	115.02	450				1.10	1.900	109.19	35.00%
---		MH (321)	MH323							0.00	1.95	11.01	0.25	11.26	99.15	116.20	169.83	192.95			0.00	192.95	311.95	28.70	450				1.10	1.900	119.01	38.15%
---	323	MH323	MH (185)					1.77		3.94	19.03	16.13	0.35	16.49	80.06	93.74	136.87	1,523.34		0.00	147.20	1,670.54	2,332.02	26.99	1500				0.10	1.278	661.49	28.37%
---		MH (185)	MH (186)							0.00	19.03	16.49	0.48	16.97	79.05	92.55	135.11	1,503.95			147.20	1,651.15	2,332.02	37.18	1500				0.10	1.278	680.87	29.20%
---		MH (186)	MH326							0.00	19.03	16.97	0.53	17.50	77.69	90.95	132.77	1,478.13			147.20	1,625.33	2,332.02	40.46	1500				0.10	1.278	706.70	30.30%
---	326	MH326	MH (188)					3.83		8.52	32.82	18.59	0.60	19.18	73.51	86.04	125.57	2,412.31		0.00	147.20	2,559.51	3,006.86	48.73	1650				0.10	1.362	447.36	14.88%
---		MH (188)	MH205							0.00	32.82	19.18	1.02	20.21	72.10	84.38	123.13	2,365.82			147.20	2,513.02	3,006.86	83.74	1650				0.10	1.362	493.85	16.42%
Codd's Road	201	MH201	MH (324)					0.31		0.69	0.69	10.00	1.76	11.76	104.19	122.14	178.56	71.83			0.00	71.83	91.46	84.87	375				0.25	0.802	19.62	21.45%
Codd's Road		MH (324)	MH205							0.00	0.69	11.76	1.49	13.25	95.72	112.16	163.90	65.99			0.00	65.99	91.46	71.59	375				0.25	0.802	25.46	27.84%
---		MH205	MH (386)							0.00	33.50	20.21	0.05	20.25	69.80	81.68	119.17	2,338.54		98.00	245.20	2,583.74	4,754.27	6.00	1650				0.25	2.154	2170.53	45.65%
---		MH (386)	MH (190)							0.00	33.50	20.25	0.11	20.37	69.70	81.56	119.00	2,335.18			245.20	2,580.38	4,754.27	14.70	1650				0.25	2.154	2173.89	45.73%
---	205	MH (190)	MH (191)	2.53						1.41	34.91	20.37	0.58	20.95	69.45	81.27	118.58	2,424.69			245.20	2,669.89	4,754.27	75.27	1650				0.25	2.154	2084.38	43.84%
---		MH (191)	MH (192)							0.00	34.91	20.95	0.37	21.32	68.23	79.84	116.47	2,382.04			245.20	2,627.24	4,754.27	48.00	1650				0.25	2.154	2127.03	44.74%
---		MH (192)	MH (193)							0.00	34.91	21.32	1.08	22.41	67.48	78.95	115.17	2,355.70			245.20	2,600.90	4,754.27	140.00	1650				0.25	2.154	2153.37	45.29%
---	</																															



IBI Group
400-333 Preston Street
Ottawa, Ontario
K1S 5N4

STORM SEWER DESIGN SHEET

PROJECT: FORMER CFB ROCKCLIFFE
LOCATION: CITY OF OTTAWA
CLIENT: CANADA LANDS COMPANY

LOCATION				AREA (Ha)						RATIONAL DESIGN FLOW											SEWER DATA										
STREET	AREA ID	FROM MH	TO MH	C= 0.20	C= 0.50	C= 0.70	C= 0.75	C= 0.80	C= 0.90	IND 2.78AC	CUM 2.78AC	INLET (min)	TIME IN PIPE	TOTAL (min)	i (5) (mm/hr)	i (10) (mm/hr)	i (100) (mm/hr)	5yr PEAK FLOW (L/s)	10yr PEAK FLOW (L/s)	FIXED FLOW (L/s)		DESIGN FLOW (L/s)	CAPACITY (L/s)	LENGTH (m)	PIPE SIZE (mm)			SLOPE (%)	VELOCITY (m/s)	AVAIL CAP (5yr)	
																						IND	CUM			DIA	W	H			(L/s)
	SDA2	MH338	MH (339)			3.54				6.89	7.62	11.78	1.33	13.11	95.64	112.06	163.76	729.01		0.00	0.00	729.01	944.29	114.46	900			0.25	1.438	215.28	22.80%
---		MH (339)	MH (340)							0.00	7.62	13.11	0.40	13.51	90.21	105.68	154.38	687.65			0.00	687.65	944.29	34.49	900			0.25	1.438	256.64	27.18%
---		MH (340)	MH (341)							0.00	7.62	13.51	0.47	13.97	88.71	103.91	151.79	676.19			0.00	676.19	944.29	40.17	900			0.25	1.438	268.10	28.39%
---		MH (341)	MH (342)							0.00	7.62	13.97	0.47	14.44	87.02	101.93	148.88	663.37			0.00	663.37	944.29	40.24	900			0.25	1.438	280.93	29.75%
---		MH (342)	MH (343)							0.00	7.62	14.44	0.71	15.15	85.41	100.03	146.09	651.05			0.00	651.05	944.29	60.97	900			0.25	1.438	293.24	31.05%
---		MH (343)	MH (344)							0.00	7.62	15.15	0.37	15.52	83.08	97.30	142.08	633.33			0.00	633.33	944.29	31.89	900			0.25	1.438	310.96	32.93%
---		MH (344)	MH331							0.00	7.62	15.52	0.90	16.42	81.92	95.93	140.07	624.48			0.00	624.48	944.29	77.80	900			0.25	1.438	319.81	33.87%
---	--	MH331	MH332							0.00	13.09	16.42	0.36	16.78	79.24	92.77	135.44	1,037.30		0.00	0.00	1,037.30	1,689.20	55.85	900			0.80	2.572	651.90	38.59%
---		MH332	MH333							0.00	13.09	16.78	0.65	17.43	78.21	91.57	133.68	1,023.90			0.00	1,023.90	1,689.20	100.00	900			0.80	2.572	665.30	39.39%

---	183	MH241	MH242					0.13		0.29	0.29	10.00	0.93	10.93	104.19	122.14	178.56	30.12			0.00	30.12	62.04	68.00	250			1.00	1.224	31.91	51.44%
---	175	MH243	MH242			0.69				1.34	1.34	10.00	1.27	11.27	104.19	122.14	178.56	139.90			0.00	139.90	168.64	113.00	375			0.85	1.479	28.73	17.04%
---	242	MH242	MH (218)					0.89		1.98	3.61	11.27	0.38	11.65	97.92	114.75	167.70	353.60		0.00	0.00	353.60	759.45	46.80	675			0.75	2.056	405.85	53.44%
---		MH (218)	MH244							0.00	3.61	11.65	0.42	12.08	96.21	112.73	164.74	347.42			0.00	347.42	759.45	52.32	675			0.75	2.056	412.03	54.25%
---	235	MH235	MH210					1.03		2.29	2.29	10.00	0.46	10.46	104.19	122.14	178.56	238.68			0.00	238.68	347.53	43.37	525			0.60	1.555	108.85	31.32%
---		MH210	MH244							0.00	2.29	10.46	0.84	11.31	101.80	119.32	174.42	233.20			0.00	233.20	347.53	78.74	525			0.60	1.555	114.33	32.90%
---	244	MH244	MH (240)	2.24				0.41		2.16	8.06	12.08	0.93	13.01	94.37	110.57	161.57	760.54		0.00	0.00	760.54	1,101.81	134.65	750			0.90	2.416	341.27	30.97%
---		MH (240)	MH258							0.00	8.06	13.01	0.53	13.54	90.61	106.15	155.07	730.23			0.00	730.23	1,101.81	77.04	750			0.90	2.416	371.58	33.72%
---	257	MH257	MH256					1.40		3.11	3.11	10.00	1.47	11.47	104.19	122.14	178.56	324.42			0.00	324.42	367.27	71.26	750			0.10	0.805	42.86	11.67%
---	256	MH256	MH258					1.46		3.25	6.36	11.47	1.09	12.56	97.00	113.67	166.12	616.98			0.00	616.98	821.24	117.34	750			0.50	1.801	204.27	24.87%
---	258	MH258	MH (243)					2.83		6.29	20.71	13.54	0.28	13.82	88.60	103.79	151.60	1,835.28		0.00	0.00	1,835.28	2,490.17	28.39	1350			0.20	1.685	654.88	26.30%
---		MH (243)	MH (266)							0.00	20.71	13.82	0.90	14.72	87.58	102.59	149.84	1,814.15			0.00	1,814.15	2,490.17	91.02	1350			0.20	1.685	676.01	27.15%
---		MH (266)	MH252							0.00	20.71	14.72	0.14	14.85	84.48	98.94	144.49	1,749.89			0.00	1,749.89	2,490.17	13.86	1350			0.20	1.685	740.27	29.73%
---	252	MH252	MH251					0.15		0.33	21.05	14.85	0.77	15.62	84.03	98.41	143.71	1,768.58			0.00	1,768.58	2,490.17	77.49	1350			0.20	1.685	721.58	28.98%
---	256	MH256	MH (233)					2.50		5.56	5.56	10.00	0.21	10.21	104.19	122.14	178.56	579.31			0.00	579.31	876.93	30.59	675			1.00	2.374	297.62	33.94%
---		MH (233)	MH (234)							0.00	5.56	10.21	0.23	10.44	103.07	120.82	176.62	573.08			0.00	573.08	876.93	32.54	675			1.00	2.374	303.85	34.65%
---		MH (234)	MH (235)							0.00	5.56	10.44	0.21	10.65	101.91	119.45	174.61	566.61			0.00	566.61	876.93	30.14	675			1.00	2.374	310.32	35.39%
---		MH (235)	MH (236)							0.00	5.56	10.65	0.28	10.94	100.86	118.21	172.79	560.76			0.00	560.76	876.93	40.35	675			1.00	2.374	316.17	36.05%
---		MH (236)	MH (237)							0.00	5.56	10.94	0.24	11.18	99.49	116.60	170.42	553.14			0.00	553.14	876.93	34.51	675			1.00	2.374	323.79	36.92%
---		MH (237)	MH251							0.00	5.56	11.18	0.18	11.36	98.35	115.26	168.44	546.80			0.00	546.80	876.93	25.72	675			1.00	2.374	330.13	37.65%
---	251	MH251	MH (270)	0.64				0.12		0.62	27.23	15.62	0.20	15.82	81.60	95.55	139.52	2,222.04		0.00	0.00	2,222.04	4,313.09	35.44	1350			0.60	2.919	2091.05	48.48%
---		MH (270)	MH250							0.00	27.23	15.82	0.18	16.01	80.99	94.83	138.46	2,205.29			0.00	2,205.29	4,313.09	32.23	1350			0.60	2.919	2107.80	48.87%
Hemlock Road	230	MH234	MH (273)					2.66		5.92	5.92	10.00	0.25	10.25	104.19	122.14	178.56	616.39			0.00	616.39	876.93	35.00	675			1.00	2.374	260.54	29.71%
Hemlock Road		MH (273)	MH (274)							0.00	5.92	10.25	0.27	10.52	102.91	120.63	176.34	608.81			0.00	608.81	876.93	38.92	675			1.00	2.374	268.12	30.57%
Hemlock Road		MH (274)	MH235							0.00	5.92	10.52	0.21	10.73	101.53	119.00	173.95	600.63			0.00	600.63	876.93	30.00	675			1.00	2.374	276.30	31.51%
Hemlock Road	235	MH235	MH (262)					1.15		2.56	8.47	10.73	1.13	11.86	100.49	117.78	172.15	851.50			0.00	851.50	1,045.56	91.62	975			0.20	1.357	194.06	18.56%
Hemlock Road		MH (262)	MH245							0.00	8.47	11.86	0.61	12.47	95.32	111.69	163.21	807.68			0.00	807.68	1,045.56	49.80	975			0.20	1.357	237.89	22.75%
Hemlock Road	245	MH245	MH (223)					0.37		0.82	9.30	12.47	0.27	12.74	92.75	108.66	158.77	862.21			0.00	862.21	2,626.46	47.67	1050			0.85	2.938	1764.25	67.17%
Hemlock Road		MH (223)	MH212							0.00	9.30	12.74	0.26	12.99	91.66	107.38	156.89	852.10			0.00	852.10	2,626.46	45.18	1050			0.85	2.938	1774.36	67.56%
Hemlock Road		MH212	MH250							0.00	9.30	12.99	0.33	13.32	90.65	106.20	155.15	842.75			0.00	842.75	2,626.46	58.30	1050			0.85	2.938	1783.71	67.91%
Hemlock Road	250	MH250	MH (227)					0.46		1.02	37.55	16.01	0.32	16.33	80.44	94.18	137.51	3,020.37		0.00	0.00	3,020.37	5,214.57	54.46	1500			0.50	2.859	2194.19	42.08%
Hemlock Road		MH (227)	MH (228)							0.00	37.55	16.33	0.35	16.68	79.51	93.09	135.91	2,985.44			0.00	2,985.44	5,214.57	60.48	1500			0.50	2.859	2229.12	42.75%
Hemlock Road		MH (228)	MH271							0.00	37.55	16.68	0.33	17.01	78.50	91.91	134.17	2,947.69			0.00	2,947.69	5,214.57	56.40	1500			0.50	2.859	2266.88	43.47%
Hemlock Road	271	MH271	MH272					0.58		1.29	38.84	17.01	0.32	17.33	77.59	90.83	132.60	3,013.51			0.00	3,013.51	4,545.95	47.91	1500			0.38	2.492	1532.44	33.71%
Hemlock Road	271	MH272	HW					0.58		1.29	40.13	17.33	0.05	17.38	76.72	89.82	131.10	3,078.82			0.00	3,078.82	4,545.95	7.58	1500			0.38	2.492	1467.14	32.27%
---	261	MH360	HW-3					1.77		3.94	3.94	10.00	0.68	10.68	104.19	122.14	178.56	410.15				410.15	549.49	100.00	525			1.50	2.459	139.34	25.36%

Water Quality Volume Calculations

Eastern SWM Facility

The Stormwater Management Facility is being designed as a wet pond at an Enhanced Level of Protection.

Drainage area = 160.58 ha (see Table 1)

Total imperviousness ratio = 63% (see Table 1)

From MOE Stormwater Management Planning and Design Manual, March 2003. p. 3-10:

Protection Level	SWMP Type	Storage Volume (m ³ /ha) for Impervious Level	
		55 %	70 %
Enhanced 80% long-term S.S. removal	Wet Pond	190	225

Total storage volume for wet pond:

$$\begin{aligned} Y_3 &= Y_2 + (X_3 - X_2)[(Y_2 - Y_1)/(X_2 - X_1)] \\ &= 190 + (225 - 190)[(63 - 55)/(70 - 55)] \\ &= 208.7 \text{ m}^3/\text{ha} \end{aligned}$$

An imperviousness ratio of 66% corresponds to a total storage volume of 209 m³/ha.

If extended detention = 40 m³/ha

Then permanent storage = (209 m³/ha – 40 m³/ha) = 169 m³/ha

Therefore:

Permanent storage volume = 169 m³/ha x 160.58 ha = 27138.02 m³ = 2.72 ha-m

Extended detention volume = 40 m³/ha x 160.58 ha = 6423.2 m³ = 0.642 ha-m

Table 1: Total Area and Total Weighted imperviousness for Water Quality Calculation – Eastern SWM Facility
(refer to Table 6.13 and 6.14 for summary of hydrological parameters)

Area ID	Area (ha)	Weighted Total Imperviousness (%, TIMP)	Area (ha) x TIMP
Tributary To Eastern SWM Facility			
PH3B	3.11	0*	0.00
PH3D	5.07	81	410.67
PH3E	0.44	79	34.76
PH3F	4.36	79	344.44
PH3G	8.21	83	681.43
PH3H	6.92	80	553.60
PH3I	2.38	86	204.68
PH3J	5.23	64	334.72
PH2A	1.93	86	165.98
PH2B	2.5	86	215.00
PH2C	2.53	0*	0.00
PH2D	1.14	0*	0.00
PH2J	5.14	0*	0.00
PH2L	0.49	86	42.14
PH1A	16.91	81	1369.71
PH1B	5.81	74	429.94
PH1C	6.1	0*	0.00
PH1D	1.15	0*	0.00
PH1E	3.53	86	303.58
PH1F	8.53	69	588.57
EXT1	1.52	71	107.92
EXT9	2.18	71	154.78
BRM2	7.04	71	499.84
BRMSWF	1.47	0*	0.00
BRMR1	18.65	71	1324.15
EXT-NRC	18.39	71	1305.69
EXTE1 (SWM Block)	8.52	0*	0.00
EXT7	11.33	86	974.38
Total Area (ha) =		Sum of Area (ha) X TIMP =	10045.98
Total Weighted Imperviousness (water Quality) =			63

Note: * In rural areas, imperviousness is set at zero.

Water Quality Volume Calculations

Western SWM Facility

The Stormwater Management Facility is being designed as a wetland at an Enhanced Level of Protection.

Drainage area = 44.80 ha (see Table 2)

Total imperviousness ratio = 35% (see Table 2)

From MOE Stormwater Management Planning and Design Manual, March 2003. p. 3-10:

Protection Level	SWMP Type	Storage Volume (m ³ /ha) for Impervious Level
		35 %
<i>Enhanced</i> 80% long-term S.S. removal	Wet Pond	140

Total storage volume for wetland:

$$Y_3 = 140 \text{ ha-m}$$

An imperviousness ratio of 35% corresponds to a total storage volume of 140 m³/ha.

If extended detention = 40 m³/ha

Then permanent storage = (140 m³/ha – 40 m³/ha) = 100 m³/ha

Therefore:

Permanent storage volume = 100 m³/ha x 44.80 ha = 4480 m³ = 0.45 ha-m

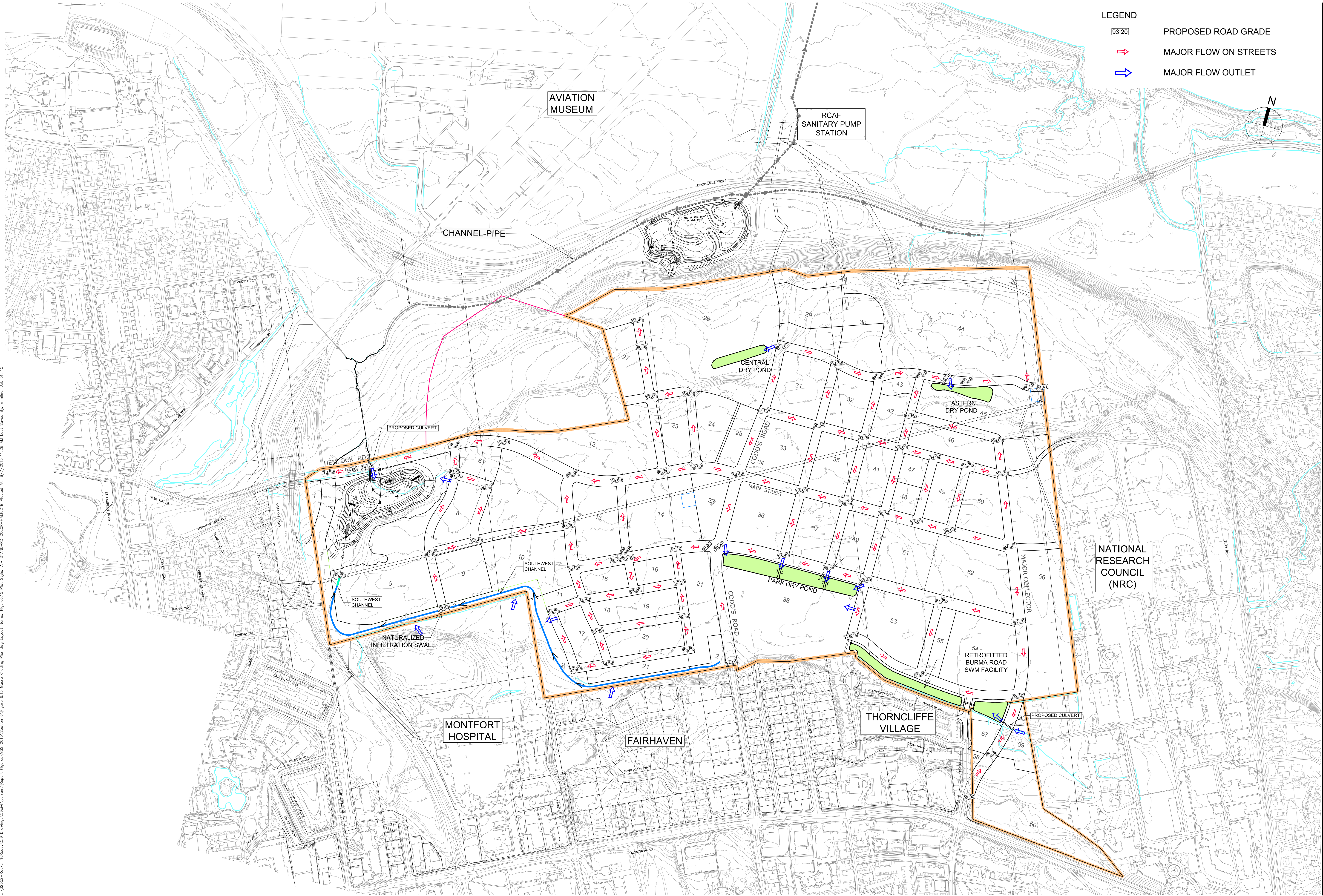
Extended detention volume = 40 m³/ha x 44.80 ha = 1792 m³ = 0.18 ha-m

Table 2: Total Area and Total Weighted imperviousness for Water Quality Calculation – Western SWM Facility
(refer to Table 6.13 and 6.14 for summary of hydrological parameters)

Area ID	Area (ha)	Weighted total Imperviousness (%, TIMP)	Area (ha) x TIMP
Tributary To Western SWM Facility			
PH2E	16.11	70	1127.70
PH2F	1.09	86	93.74
PH2G	1.77	86	152.22
PH2H (SWM Block)	4.52	0*	0.00
PH2K	1.57	86	135.02
EXM	2.02	31	62.62
EXT4	7.84	0*	0.00
EXT5	1.46	0*	0.00
EXT3	2.25	0*	0.00
EXT2	6.17	0*	0.00
Total Area (ha)	44.8	Sum of Area (ha) X TIMP	1571.30
Total Weighted Imperviousness (water Quality) =			35

Note: *In rural areas, imperviousness is set at zero.

A:\32952-rockcliffe\Drawings\32952\Section 6\Figure 6.15 Macro Grading Plan.dwg Layout Name: Figure 6.15 Plot Style: AA STANDARD COLOR-HALF-CTB Plotted At: 8/7/2015 11:28 AM Last Saved By: mmh, Jul. 31, 15



Sheet No.

Drawing Title

Project Title

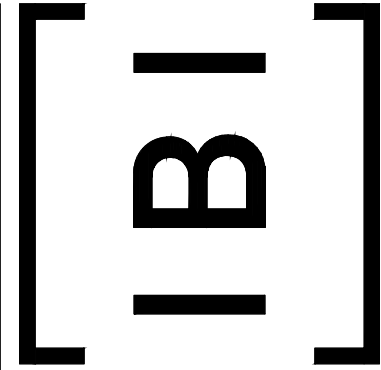
Scale

0 100 200

FIGURE 6.15

MACRO
GRADING PLAN

FORMER CFB ROCKCLIFFE
MASTER SERVICING STUDY





Street Segment Velocity x Depth Calculation

Iteration equation:

Velocity:

$$v_x = v_{min} + \frac{Q_x - Q_{min}}{Q_{max} - Q_{min}} (v_{max} - v_{min})$$

Depth:

$$d_x = d_{min} + \frac{Q_x - Q_{min}}{Q_{max} - Q_{min}} (d_{max} - d_{min})$$

100 Year 3 Hour Chicago Storm																		
					SWMHYMO (32952VXD.out)					Calculation Sheet: Overflow for Typical Road Ponding Area					Continuous Grade (SWMHYMO 32952VXD.out)			
Area ID (Dummy Segment, if applicable)	Road ROW Section	Longitudinal Slope (%)	Overflow Flowrate		Flowrate (cms)		Velocity (m/s)			Flowrate (cms)		Depth (m)			Depth (m)			Velocity x Depth
			Qx (l/s)	Qx (cms)	Qmin	Qmax	vmin	vmax	vx	Qmin	Qmax	dmin	dmax	dx	dmin	dmax	dx	(m ² /s)
PH3H(323 TO 320)	20	1.49	1237	1.24	1.00	1.32	1.61	1.80	1.75	n/a	n/a	n/a	n/a	n/a	0.14	0.15	0.15	0.26
PH1A (163 TO 130)	20	0.5	808	0.81	0.77	0.98	1.04	1.14	1.06	n/a	n/a	n/a	n/a	n/a	0.15	0.16	0.15	0.16
PH1A (130 TO 115)	20	0.58	1286	1.29	1.06	1.32	1.22	1.30	1.29	1.28	1.35	0.23	0.24	0.23	n/a	n/a	n/a	0.30
PH1A (125 TO 130)	26	0.73	1297	1.30	1.15	1.43	1.04	1.09	1.07	n/a	n/a	n/a	n/a	n/a	0.19	0.21	0.20	0.21
PH3G (155 TO 150)	26	0.54	500	0.50	0.48	0.60	0.72	0.78	0.73	0.49	0.52	0.17	0.17	0.17	n/a	n/a	n/a	0.12
PH2E (230 TO 235)	26	0.71	673	0.67	0.55	0.69	0.82	0.89	0.88	n/a	n/a	n/a	n/a	n/a	0.14	0.15	0.15	0.13
PH1F (183 TO 185)	20	1.65	893	0.89	0.76	1.05	1.51	1.69	1.59	n/a	n/a	n/a	n/a	n/a	0.12	0.14	0.13	0.21
PH1F (190 TO 185)	20	1.19	595	0.60	0.47	0.65	1.19	1.28	1.25	n/a	n/a	n/a	n/a	n/a	0.11	0.12	0.12	0.15
PH2E (251 TO 250)	20	2.86	2290	2.29	2.21	2.61	1.62	1.67	1.63	n/a	n/a	n/a	n/a	n/a	0.20	0.22	0.20	0.33
PH2E (250 TO 271)	26	3.7	3950	3.95	3.84	4.65	2.45	2.52	2.46	n/a	n/a	n/a	n/a	n/a	0.22	0.24	0.23	0.56

Master Servicing Study - Southwest Drainage Channel Design
Former CFB Rockcliffe

South West Channel Design Reach 1 (Section A-A, refer to Figure 6.25)

New Swale Section Required flow =	1170 L/s	(1.17 cms)		
From Seelye use n =	0.040		area =	1.41
Choose Slope S =	0.50 %		wp =	4.42
Ditch Bottom =	1.00 m			
Ditch slopes =	3 :1			
Water depth =	0.54 m	(depth needed to carry 1.17 cms)		
Check Ditch Capacity (Q) :			Ditch Bottom =	86.50 m
	Q = 1.17 cms	and Velocity = 0.83 m/s	Ditch Top =	88.00 m
			Freeboard =	0.96 m

South West Channel Design Reach 2 (Section B-B, refer to Figure 6.25)

New Swale Section Required flow =	2610 L/s	(2.61 cms)		
From Seelye use n =	0.040		area =	1.78
Choose Slope S =	1.40 %		wp =	5.04
Ditch Bottom =	1.50 m			
Ditch slopes =	3 :1			
Water depth =	0.56 m	(depth needed to carry 2.61 cms)		
Check Ditch Capacity (Q) :			Ditch Bottom =	83.50 m
	Q = 2.63 cms	and Velocity = 1.48 m/s	Ditch Top =	85.50 m
			Freeboard =	1.44 m

South West Channel Design Reach 3

New Swale Section Required flow =	3440 L/s	(3.44 cms)		
From Seelye use n =	0.040		area =	2.88
Choose Slope S =	0.75 %		wp =	6.79
Ditch Bottom =	3.00 m			
Ditch slopes =	3 :1			
Water depth =	0.60 m	(depth needed to carry 3.44 cms)		
Check Ditch Capacity (Q) :			Ditch Bottom =	80.40 m
	Q = 3.52 cms	and Velocity = 1.22 m/s	Ditch Top =	82.60 m
			Freeboard =	1.60 m

South West Channel Design Reach 4

New Swale Section Required flow =	5768 L/s	(5.77 cms)		
From Seelye use n =	0.040		area =	3.08
Choose Slope S =	1.70 %		wp =	6.98
Ditch Bottom =	3.00 m			
Ditch slopes =	3 :1			
Water depth =	0.63 m	(depth needed to carry 5.77 cms)		
Check Ditch Capacity (Q) :			Ditch Bottom =	78.40 m
	Q = 5.82 cms	and Velocity = 1.89 m/s	Ditch Top =	79.80 m
			Freeboard =	0.77 m

$$Q = A \cdot (1.49/n) \cdot R^{2/3} \cdot S^{1/2}$$

where:

A = cross sectional area in Sq. m

n = friction coefficient

R = hydraulic radius = A / wetted perimeter (wp) in m

S = ditch slope in %

Master Servicing Study - NRC Drainage Swale Design
Former CFB Rockcliffe

NRC Drainage Ditch Commercial Lands

Commercial Lands Ditch For NRC Surface Drainage

New Swale Section	Required flow = 5700 l/s	5.70 Cu m/sec		
From Seelye use n =	0.050		area=	4.95
choose: slope S =	0.65 %		wp=	8.01
Ditch Bottom	3.00 metres	Max Easement width =	9.15 m	
Ditch slopes	2.50 :1			
Water depth	0.93 metres (depth needed to carry 5.70 Cu. M/sec)			
Check Ditch Capacity (Q)				
Q =	5.80 Cu M/sec	and Velocity =	1.17 M/s	

$$Q = A \cdot (1.49/n) \cdot R^{2/3} \cdot S^{1/2}$$

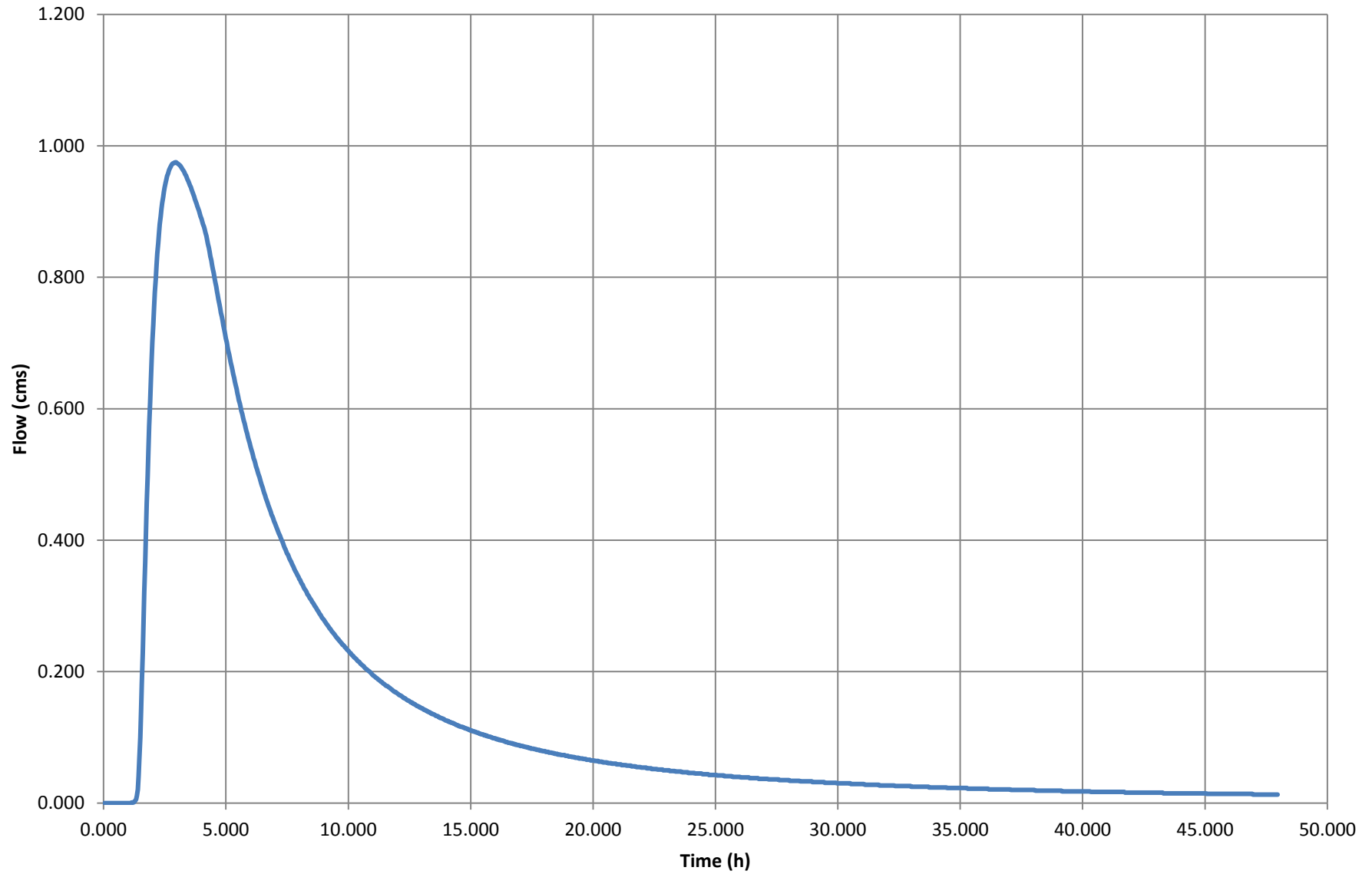
where:

A = cross sectional area in Sq. m

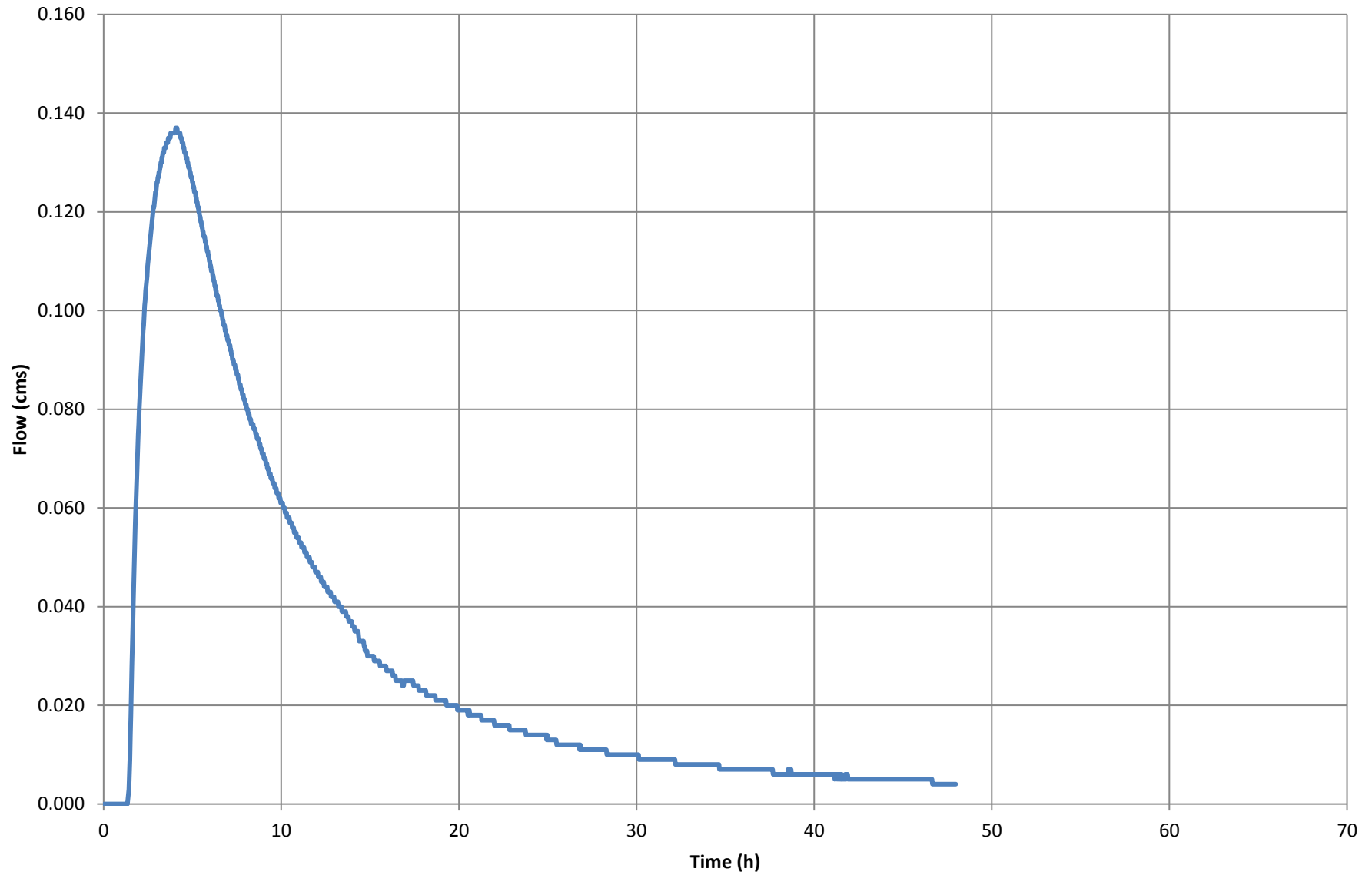
n = friction coefficient

R = hydraulic radius = A/wetted perimeter (wp) in m

Eastern SWM Facility 25 mm Hydrograph Out of Pond



Western SWM Facility 25 mm Hydrograph Out of Pond



Eastern Creek Baseflow Augmentation Calculation

Existing Conditions

Area to Eastern Creek (refer to Figure 2.16): $(36.34 \text{ ha} + 24.68 \text{ ha}) = 61.02 \text{ ha}$

Under post-development conditions, there is no proposed development of Area EXTE2 (refer to Figure 6.12), which measures 15.13 ha, so for the purposes of this calculation, consider: $(61.02 \text{ ha} - 15.13 \text{ ha}) = 45.89 \text{ ha}$

Considering annual infiltration rate per the Aquafor Beech water budget analysis (MSS Table 6.4): 235 mm/year

Existing conditions volumetric infiltration:

$$\begin{aligned} &= 235 \frac{\text{mm}}{\text{year}} \times \frac{1\text{m}}{1000\text{mm}} \times 45.89 \text{ ha} \times \frac{10000\text{m}^2}{1\text{ha}} \\ &= 107,842 \frac{\text{m}^3}{\text{year}} \end{aligned}$$

It is assumed that approximately 50% of the volumetric infiltration will participate in generating baseflow feeding the Eastern Creek:

$$\begin{aligned} &= 107,842 \frac{\text{m}^3}{\text{year}} \times 50\% \\ &= 53,741 \frac{\text{m}^3}{\text{year}} \end{aligned}$$

Expressed on a per hectare basis, the existing conditions volumetric infiltration:

$$\begin{aligned} &= \frac{\left(53,741 \frac{\text{m}^3}{\text{year}}\right)}{45.89\text{ha}} \\ &= 1171 \frac{\text{m}^3}{\text{year}} \text{ per hectare} \end{aligned}$$

Post-Development Conditions

Two drainage areas contribute flow to Eastern Creek, PH3A and EXTE2 (refer to Figure 6.12).

Referring to the 25 mm SWMHYMO simulation results, the runoff coefficients for the drainage areas are as follows:

Area ID	Land Use	Area (ha)	Volumetric Runoff Coefficient
PH3A	Urban	6.68	$0.717 \approx 0.72$ ($\therefore \approx 0.28$ infiltrates)
EXTE2	Rural (no proposed change)	15.13	$0.174 \approx 0.17$ ($\therefore \approx 0.83$ infiltrates)

From the above it is concluded that an urban development can produce approximately 34% of the infiltration in comparison with a rural area.

The post-development urban area contributing flow to the Eastern Creek, PH3A measures: 6.68 ha

The corresponding infiltrated volume for this urban area:

$$= 6.68 \text{ ha} \times \frac{1171 \text{ m}^3/\text{year}}{\text{ha}} \times 0.34$$

$$= 2660 \frac{\text{m}^3}{\text{year}}$$

The baseflow compensation to the Eastern Creek is therefore:

$$= V_{Existing} - V_{PostDev}$$

$$= (53,741 \frac{\text{m}^3}{\text{year}}) - (2660 \frac{\text{m}^3}{\text{year}})$$

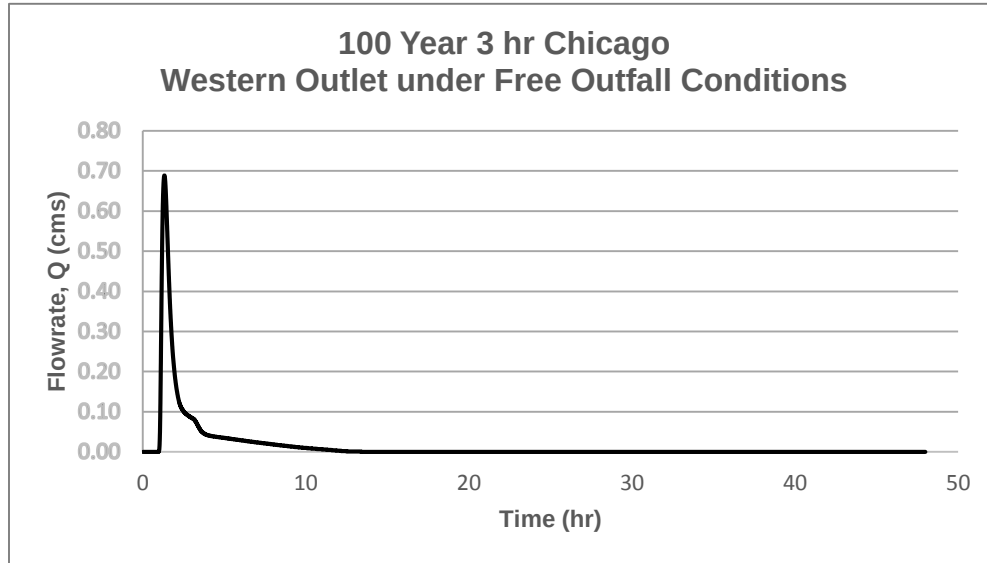
$$= 51,081 \frac{\text{m}^3}{\text{year}}$$

It is recommended that this be confirmed at the detailed design stage, supported by continuous modeling.

Boundary Condition for Western Creek Outlet

Step 1. Run XPSWMM model assuming “Free Outfall” with the depth criterion “minimum yc_yn”. Where yc is critical depth and yn is normal depth.

Step2. Export Outflow vs Time rating curve from “Aviation CH” link between DROP and NODE220 Nodes (see 100 year 3 hour Chicago example below).



Step3. Calculate a ratio based on flow rate for each time step from the Outflow-Time curve from Step 2. See equation below:

Ratio (R_x):

$$R_x = \frac{Q_x - Q_{min}}{Q_{max} - Q_{min}}$$

Where:

- Q_x : Flow rate at time x
- Q_{min} : Minimum flow rate from all time steps
- Q_{max} : Maximum flow rate from all time steps

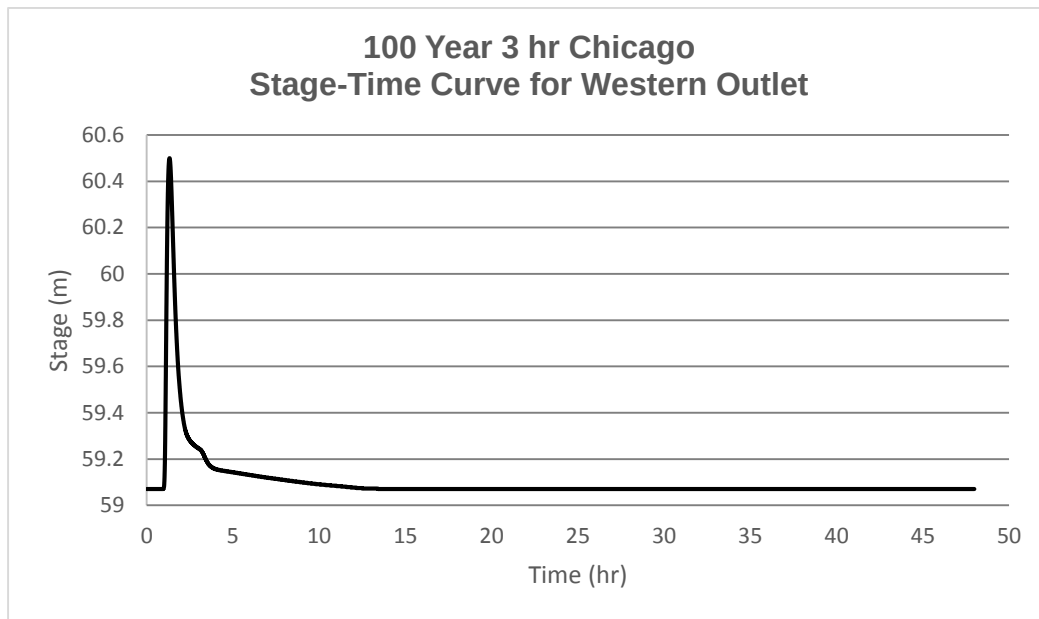
Step4. Using the invert of the Western Creek at approximately 113 m downstream of the Aviation culvert (elevation 59.07 m), the maximum possible Western Creek water level (60.50 m), which corresponds to the existing road elevation at the culvert crossing further downstream, and the ratio determined in Step 3, create a Stage vs Time relationship at each time step. See equation below:

Outlet Stage (m):

$$H_x = R_x (Cr_{WL} - Cr_{inv}) + Cr_{inv}$$

Where:

- R_x : Ratio from Step 3
- Cr_{wl} : Maximum Western Creek water level (m)
- Cr_{inv} : Western Creek invert at approximately 113m downstream of the Aviation culvert (node Drop)



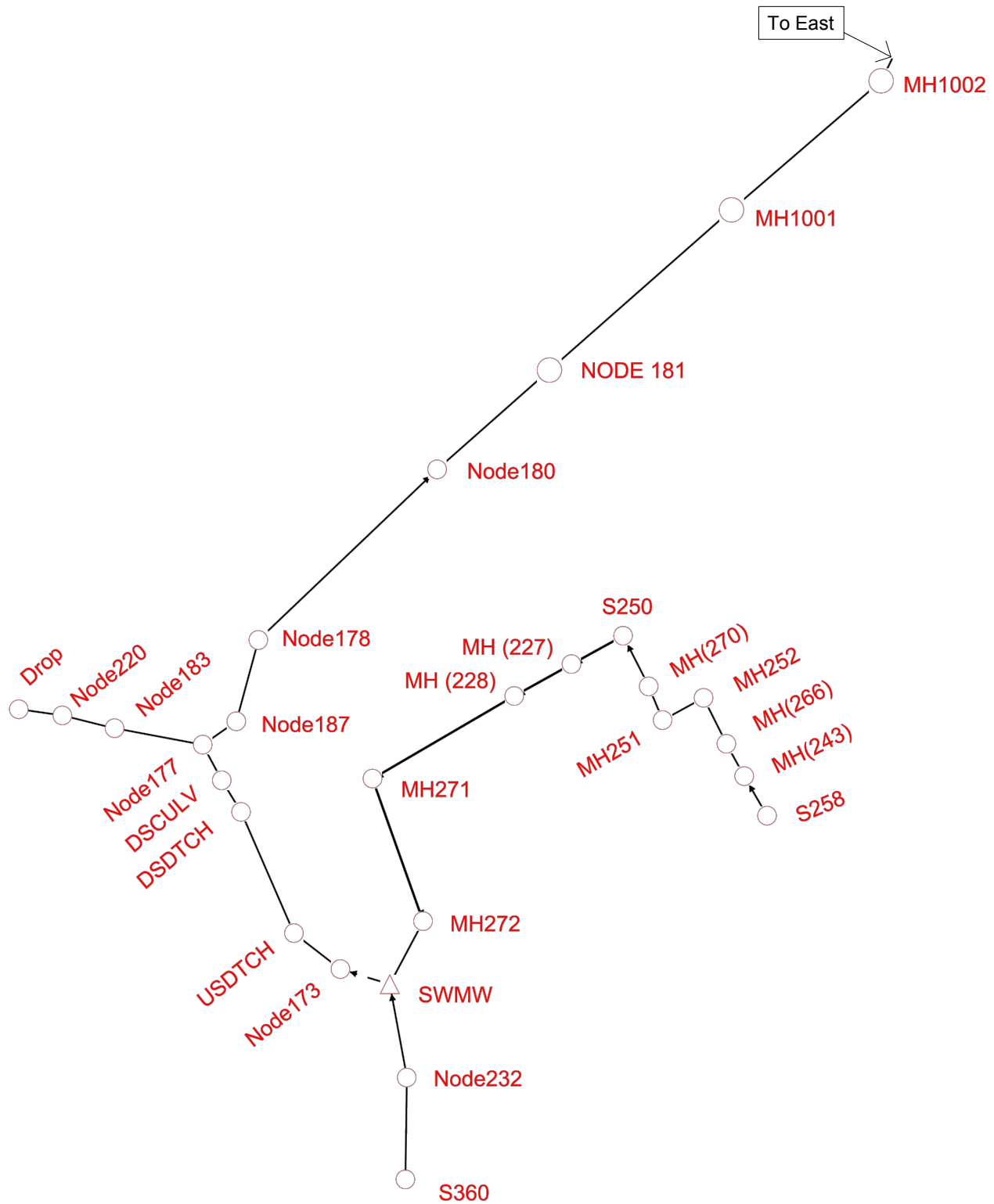
Step5: Copy Stage vs Time curve created in Step 4 into XPSWMM via Node DROP ->Outfall -> 3.3 User Stage History -> Coordinates. Re-run XPSWMM with User Stage History specified as the outlet condition.

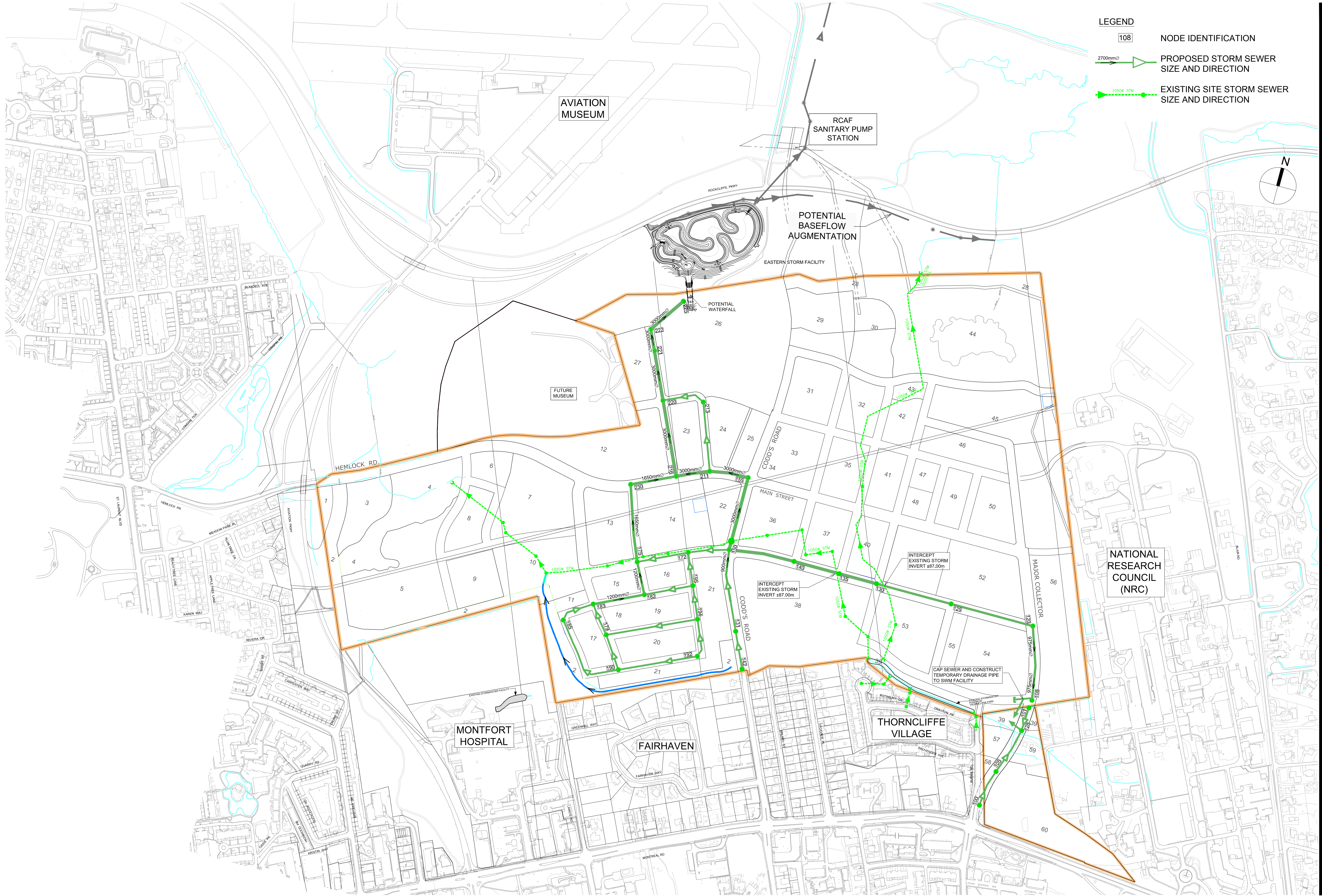
The same process is followed for all the storm events modeled.

Hydraulic Grade Line

XPSWMM Node ID	MH No.	Proposed Ground Road (m)	USF (m)	100 year 3 hour Chicago + 20%		100 year 24 hour SCS		July 1, 1979		August 1988		August 1996	
				HGL (m)	USF - HGL (m)	HGL (m)	USF - HGL (m)	HGL (m)	USF - HGL (m)	HGL (m)	USF - HGL (m)	HGL (m)	USF - HGL (m)
EASTERN SWM FACILITY													
ESTSWM	N/A	N/A	N/A	58.11	N/A	74.80	N/A	58.59	N/A	58.15	N/A	57.63	N/A
MH 226	226	82.51	80.11	71.23	8.88	75.06	5.05	71.22	8.89	71.21	8.90	71.19	8.92
S225	225	82.51	80.11	75.25	4.86	75.06	5.05	75.12	4.99	75.05	5.06	74.83	5.28
MH (194)	194	82.86	80.46	75.74	4.72	75.54	4.92	75.59	4.87	75.52	4.94	75.27	5.19
MH222	222	84.4	82.00	79.98	2.02	79.77	2.23	79.83	2.17	79.75	2.25	79.50	2.50
S221	221	86	83.60	80.60	3.00	80.39	3.21	80.44	3.16	80.37	3.23	80.12	3.48
MH220	220	87	84.60	80.99	3.61	80.75	3.85	80.81	3.79	80.73	3.87	80.45	4.15
S216	216	88	85.60	81.73	3.87	81.39	4.21	81.47	4.13	81.36	4.24	81.02	4.58
MH (161)	161	88.4	86.00	83.90	2.10	83.65	2.35	83.70	2.30	83.63	2.37	83.34	2.66
S211	211	89	86.60	84.03	2.57	83.76	2.84	83.81	2.79	83.74	2.86	83.44	3.16
MH (159)	159	88.62	86.22	84.15	2.07	83.87	2.35	83.92	2.30	83.84	2.38	83.53	2.69
MH155	155	88.4	86.00	84.52	1.48	84.19	1.81	84.25	1.75	84.17	1.83	83.81	2.19
MH(150)	150	87.75	85.35	84.95	0.40	84.55	0.80	84.62	0.73	84.52	0.83	84.13	1.22
S150	150	88.2	85.80	85.27	0.53	84.81	0.99	84.88	0.92	84.78	1.02	84.34	1.46
S140	140	88.4	86.00	85.82	0.18	85.18	0.82	85.27	0.73	85.14	0.86	84.67	1.33
MH135	135	89.2	86.80	86.02	0.78	85.30	1.50	85.40	1.40	85.27	1.53	84.81	1.99
MH130	130	90.4	88.00	86.45	1.55	85.93	2.07	85.98	2.02	85.92	2.08	85.69	2.31
MH119	119	89.65	87.25	86.84	0.41	86.34	0.91	86.39	0.86	86.32	0.93	86.05	1.20
S115	115	90	87.60	87.15	0.45	86.60	1.00	86.66	0.94	86.58	1.02	86.27	1.33
EXTBRM	128	92.75	N/A	91.32	N/A	90.21	N/A	90.24	N/A	90.20	N/A	90.08	N/A
MH230	230	85.8	83.40	81.86	1.54	81.58	1.82	81.64	1.76	81.55	1.85	81.40	2.00
MH (289)	289	85.97	83.57	81.95	1.62	81.70	1.87	81.77	1.80	81.68	1.89	81.60	1.97
S175	175	85.8	83.40	81.98	1.42	81.75	1.65	81.82	1.58	81.74	1.66	81.68	1.72
MH (193)	193	78.57	76.17	75.93	0.24	75.91	0.26	75.91	0.26	75.91	0.26	75.90	0.27
MH (192)	192	81.23	78.83	76.26	2.57	76.23	2.60	76.23	2.60	76.23	2.60	76.22	2.61
MH (191)	191	82.81	80.41	78.35	2.06	78.32	2.09	78.32	2.09	78.32	2.09	78.32	2.09
MH (190)	190	81.81	N/A	80.46	N/A	80.44	N/A	80.43	N/A	80.43	N/A	80.43	N/A
MH (386)	386	84.95	N/A	80.69	N/A	80.65	N/A	80.65	N/A	80.65	N/A	80.65	N/A
MH205	205	90.7	88.30	80.77	7.53	80.73	7.57	80.73	7.57	80.73	7.57	80.73	7.57
MH (188)	188	90.37	87.97	83.29	4.68	83.27	4.70	83.26	4.71	83.26	4.71	83.26	4.71
MH326	326	90.3	87.90	83.61	4.29	83.58	4.32	83.58	4.32	83.58	4.32	83.57	4.33
MH (186)	186	90.1	87.70	83.90	3.80	83.88	3.82	83.88	3.82	83.87	3.83	83.86	3.84
MH (185)	185	90	87.60	84.04	3.56	84.01	3.59	84.01	3.59	84.01	3.59	84.00	3.60
S323	323	90	87.60	84.14	3.46	84.11	3.49	84.11	3.49	84.10	3.50	84.09	3.51
MH (183)	183	89.08	86.68	84.17	2.51	84.13	2.55	84.14	2.54	84.13	2.55	84.12	2.56
MH (182)	182	88.45	86.05	84.20	1.85	84.16	1.89	84.16	1.89	84.16	1.89	84.14	1.91
S320	320	88	85.60	84.22	1.38	84.18	1.42	84.18	1.42	84.18	1.42	84.16	1.44
S330	330	86	N/A	85.49	N/A	85.47	N/A	85.46	N/A	85.46	N/A	85.47	N/A
MH331	331	83.5	N/A	79.99	N/A	79.99	N/A	79.98	N/A	79.98	N/A	79.98	N/A
MH332	332	82	N/A	79.50	N/A	79.49	N/A	79.49	N/A	79.49	N/A	79.49	N/A
WESTERN SWM FACILITY													
SWMW	HW	77	74.60	72.81	1.79	329	1.98	72.85	1.75	72.57	2.03	71.72	2.88
S360	261	79.5	77.10	75.04	2.06	75.04	2.06	75.04	2.06	75.04	2.06	74.68	2.42

XPSWMM Node ID	MH No.	Proposed Ground Road (m)	USF (m)	100 year 3 hour Chicago + 20%		100 year 24 hour SCS		July 1, 1979		August 1988		August 1996	
				HGL (m)	USF - HGL (m)	HGL (m)	USF - HGL (m)	HGL (m)	USF - HGL (m)	HGL (m)	USF - HGL (m)	HGL (m)	USF - HGL (m)
MH272	272	72.5	N/A	72.81	N/A	72.60	N/A	72.85	N/A	72.70	N/A	71.76	N/A
MH271	271	74.5	N/A	72.81	N/A	72.60	N/A	72.85	N/A	72.67	N/A	71.89	N/A
MH(228)	228	76.29	N/A	72.81	N/A	72.69	N/A	72.99	N/A	72.88	N/A	72.03	N/A
MH (227)	227	77.93	N/A	72.84	N/A	72.80	N/A	73.12	N/A	73.01	N/A	72.25	N/A
S250	250	79.5	77.10	74.35	2.75	74.35	2.75	74.33	2.77	74.33	2.77	74.33	2.77
MH(270)	270	79.5	77.10	75.63	1.47	75.65	1.45	75.63	1.47	75.63	1.47	75.63	1.47
MH251	251	81.2	78.80	75.86	2.94	75.86	2.94	75.86	2.94	75.86	2.94	75.86	2.94
MH252	252	82.2	79.80	76.42	3.38	76.42	3.38	76.39	3.41	76.39	3.41	76.39	3.41
MH(266)	266	82.4	80.00	76.51	3.49	76.50	3.50	76.49	3.51	76.49	3.51	76.49	3.51
MH(243)	243	82.4	80.00	76.64	3.36	76.64	3.36	76.65	3.35	76.64	3.36	76.64	3.36
S258	258	82.4	80.00	76.77	3.23	76.76	3.24	76.76	3.24	76.76	3.24	76.76	3.24





Sheet No.

Drawing Title

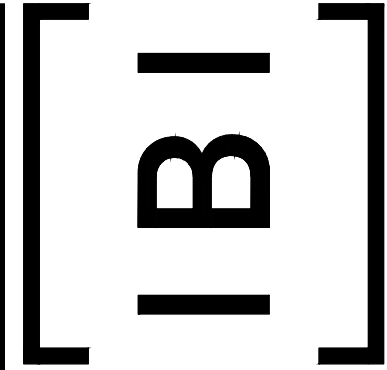
Project Title

Scale

FIGURE 6.34

RECOMMENDED PHASE 1A
STORM SEWER SYSTEM

FORMER CFB ROCKCLIFFE
MASTER SERVICING STUDY



APPENDIX F

UTILITY MEETING MINUTES



IBI Group
400–333 Preston Street
Ottawa ON K1S 5N4 Canada
tel 613 225 1311
fax 613 225 9868

Notes

To/Attention Distribution List
From Peter Kirkimtzis
Date February 7, 2014
Project No 32952 - 5.1

Subject Rockliffe Redevelopment – Utility Coordination Meeting
IBI Group Office
February 7, 2014 at 10:00am

Present

Don Schultz	CLC	dschultz@clc.ca
Krista Durie	CLC	kdurie@clc.ca
Tony Stinziano	Hydro	tonystinziano@hydroottawa.com
Mark Wojdan	Hydro	markwojdan@hydroottawa.com
Kristine McNamara	Hydro	kristinemcnamara@hydroottawa.com
Anna Borris	Enbridge	anna.borris@enbridge.com
Jeanne Dubeau	Rogers	jeanne.dubeau@rci.rogers.com
Martin Proulx	Rogers	martin.proulx@rci.rogers.com
Adam Dockstader	Bell	adam.dockstader@bell.ca
Jim Moffatt	IBI	jmoffatt@ibigroup.com
Peter Kirkimtzis	IBI	peter.kirkimtzis@ibigroup.com

Distribution All Present

Page 1 of 2

Item Discussed		Action By
1	The redevelopment will include up to 5,500 units in the mid – high density range. There will be roughly 270 single houses and roughly 75,000 square metres of commercial floor space.	Advisory
2	There will be a couple high rise apartments in the 20 storey range within the residential/commercial sector (red areas on the concept plan)	Advisory
3	The redevelopment will also include about 6 hectares owned by National Research Council (NRC) located south-east of the site.	Advisory
4	Complete build out of the redevelopment could take up to 15 – 20 years	Advisory
5	IBI will forward a phasing plan, a CAD file of the site and copies of the soils reports to all utilities.	IBI
6	CLC and IBI will meet with the City in March to discuss street cross sections. The site will consist of 18.0m, 20.0m and 26.0m ROW's. Non standard structures will be included on the cross sections such as sidewalk on both sides of the 18.0m ROW, swales and possible narrow asphalt laneways.	IBI/CLC
7	The preliminary ROW's will be circulated to the utilities for comments before the meeting with the City.	IBI

Item Discussed		Action By
8	Hydro will need to bring a high voltage line from a nearby sub-station to provide service to the site. The likely station candidates are; • Moulten sub-station through La Cite • Overbrook sub-station near St. Laurent • Hydro One sub-station on the adjacent NRC property	Hydro
9	The cost of the high voltage trunk line will be considerable and Hydro will provide CLC with a worst case economic evaluation. The price will also be offset by the number of units built within the first 5 years of construction. CLC previously estimated that about 1000 units could be built within the 5 year timeline. CLC will re-evaluate that estimate.	Hydro
10	Hydro stated that there will not be back-up power available to the site from the trunk line from Moulten sub-station due to the style of servicing provided to the sub-station. A more reliable source could be provided from the Overbrook sub-station.	Advisory
11	With its economic evaluation, Hydro will also provide an estimated timeline to build the trunk line to the site. The timeline may be in the 6 – 12 month range.	Hydro
12	CLC will require power for 2017.	Advisory
13	Hydro is currently servicing a pumping station located to the north through the Rockliffe site. A plan will be required to provide service to the pump station through the redevelopment.	Hydro/CLC
14	Enbridge will require gas loads for the site and upon receipt will begin a layout for the site. Gas will likely come from Montreal Road via Codd's Road. CLC to provide gas load summary to Enbridge.	CLC/Enbridge
15	Enbridge will also provide to CLC an economic evaluation including timelines.	Enbridge
16	Bell and Rogers have existing services on Codd's Road pole line suitable to service the site.	Advisory
17	CLC will confirm whether 3-party or 4-party trenching will be used for the site.	CLC
18	Preliminary construction schedule; Phase 1 will be the south half of the site broken into 2 sub-phases. • Phase 1A west of Codd's Road in 2015 • Phase 1B east of Codd's Road in 2016 Stage 1 will consist of roughly 680 units consisting of singles, towns semis, stacked towns and some commercial area.	Advisory

Please report any serious errors or omissions to these notes to Jim Moffatt at jmoffatt@ibigroup.com or to Peter Kirkimtzis at peter.kirkimtzis@ibigroup.com.